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LiWall Fusion and its Three Step R & D Program Toward a Reactor Development Facility

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Physics/ECE/NE 922 Seminar, The University of Wisconsin

March 24, 2008, Madison, WI

¹This work is supported by US DoE contract No. DE-AC020-76-CHO-3073.

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Abstract

The presently adopted plasma physics concept of magnetic fusion has been originated from the idea of providing low plasma edge temperature as a condition for plasma-material interaction. During 30-years of its existence this concept has shown to be not only incapable of addressing practical reactor development needs, but also to be in conflict with fundamental aspects of stationary and stable plasma.

Meanwhile, a demonstration of exceptional pumping capabilities of lithium surfaces on T-11M (1998), discovery of the quiescent H-mode regime on DIII-D (2000), and a 4 fold enhancement of the energy confinement time in CDX-U tokamak with lithium (2005), contributed to a new vision of fusion relying on high edge plasma temperature. The new concept, called LiWalls, provides a scientific basis for developing magnetic fusion.

The talk outlines 3 basic steps toward the Reactor Development Facility (RDF) with DT fusion power of 0.3-0.5 GW and a plasma volume $\simeq 30 \text{ m}^3$. Such an RDF can accomplish three reactor objectives of magnetic fusion, i.e.,

- 1. high power density $\simeq 10 \text{ MW/m}^3$ plasma regime,*
- 2. self-sufficient tritium cycle,*
- 3. neutron fluence $\simeq 10 - 15 \text{ MW}\cdot\text{year/m}^2$,*

all necessary for development of the DT power reactor. Within the same mission a better assessment of DD fuel for fusion reactors will also be possible.

The suggested program includes 3 spherical tokamaks. Two of them, ST1, ST2, are DD-machines, while the third one, ST3, represents the RDF itself with a DT plasma and neutron production.

All three devices rely on a NBI maintained plasma regime with absorbing wall boundary conditions provided by the Li based plasma facing components. The goal is to utilize the possibility of high edge temperature plasma with the super-critical ignition (SGI) regime, when the energy confinement significantly exceeds the level necessary for ignition by α -particles. In this regard all three represent Ignited Spherical Tokamaks, suggested in 2002.

Abstract

Specifically, the mission of ST1, with a size slightly larger than NSTX in PPPL but with a four times larger toroidal field, is to achieve the absorbing wall regime with confinement close to neo-classical. In particular, the milestone is $Q_{DT-equiv} \simeq 5$ corresponding to the conventional ignition criterion.

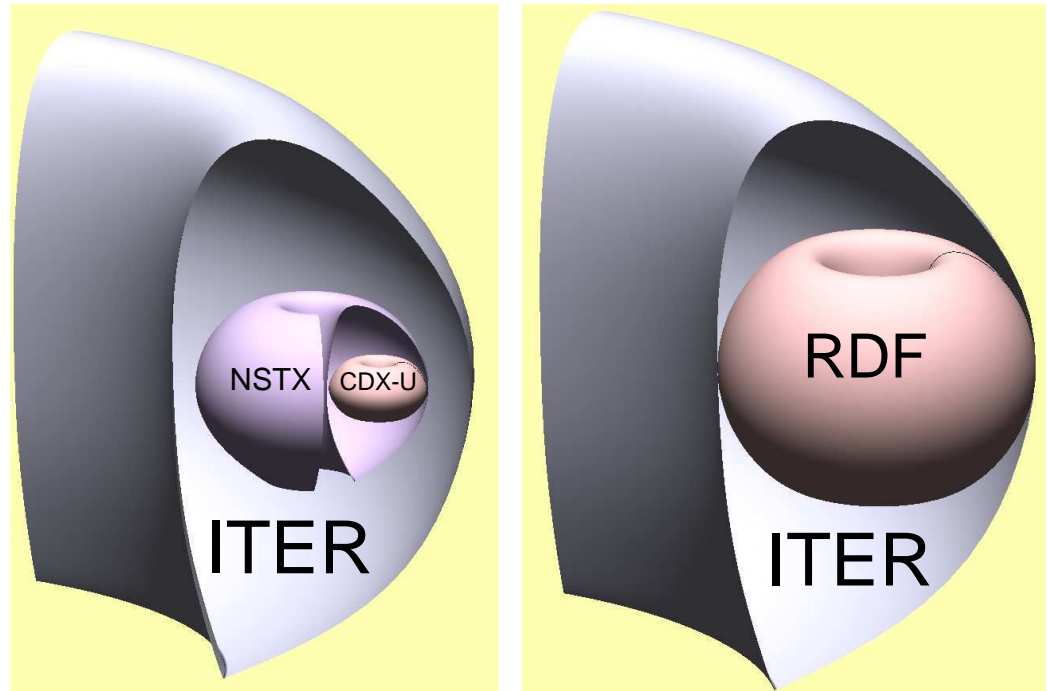
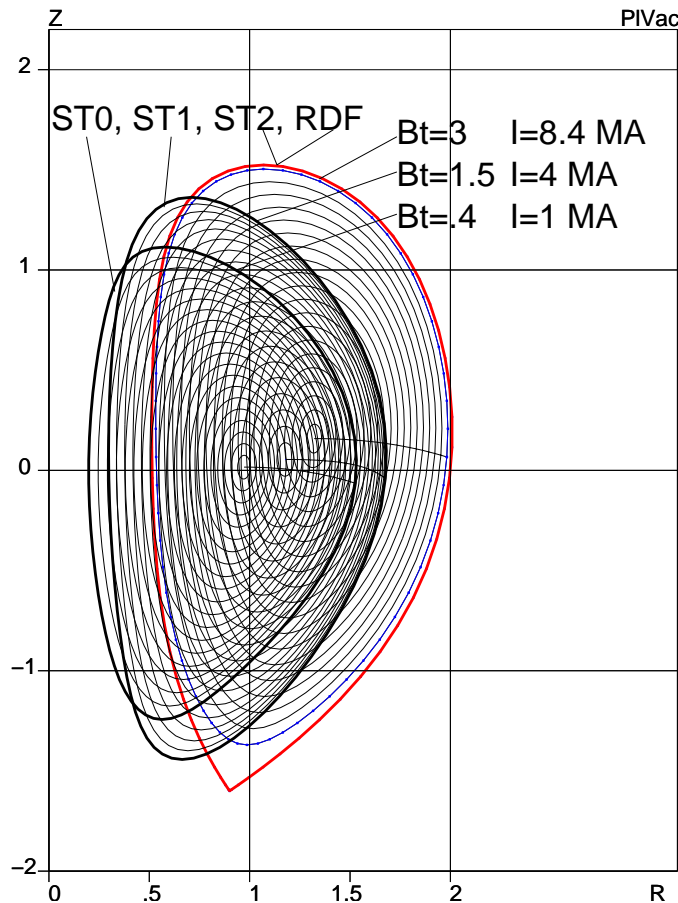
The mission of ST2, which is a full scale DD-prototype of the RDF, is the development of a stationary super-critical regime with $Q_{DT-equiv} \simeq 40 - 50$.

ST3 is a DT device with $Q_{DT} \simeq 40 - 50$ with sufficient neutron production to design the nuclear components of a power reactor. Still the mission of ST3 contains a significant plasma physics component of developing α -particle power and He ash extraction.

As a motivational step (ST0), the suggested program assumes a conversion of the existing NSTX device into a spherical tokamak with lithium plasma facing components. The demonstration of complete depletion of the plasma discharge by lithium surface pumping, first shown on T-11M, is considered as a well-defined milestone for readiness of the machine for the new plasma regime. The final mission of ST0 would be doubling or tripling the energy confinement time with respect to the current NSTX.

1 Three steps of RDF program

RDF program relies on conversion of NSTX into ST0 and on 3 new Spherical Tokamaks ST1 (DD), ST2 (DD), ST3 (DT RDF)



RDF with $P_{DT} = 0.2 - 0.5$ GW is 27 times smaller than ITER

Tritium availability sets the strategy

**The criterion of conceptual relevance
to reactor R&D is very simple:
ability of delivering**

**15 MWa/m²
of neutron fluence,
or burn-up of
1 kg(T)/m²(FW)**

**First, the Reactor Development Facility (RDF), then
the power reactor**

(ITER is capable of only 0.3-0.4 MWa/m² (burn-up of 10-15 kg of T, instead of 650 kg)

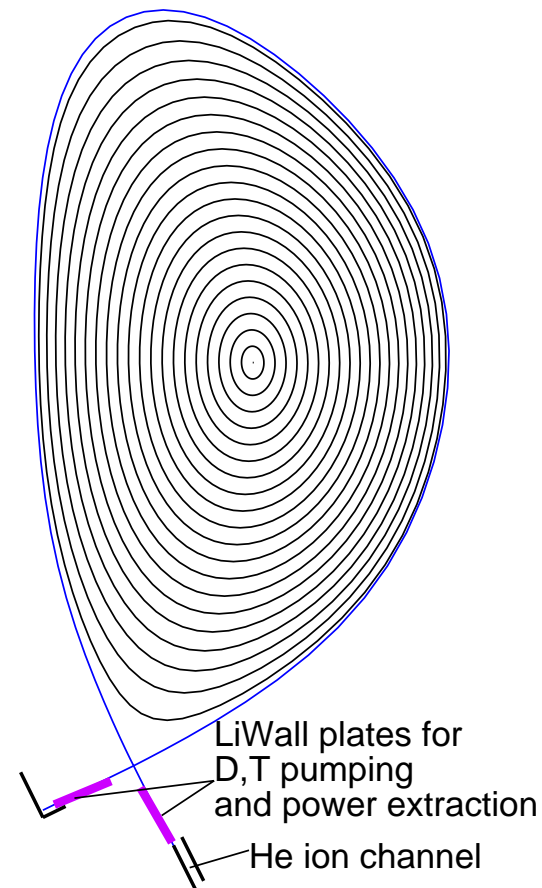
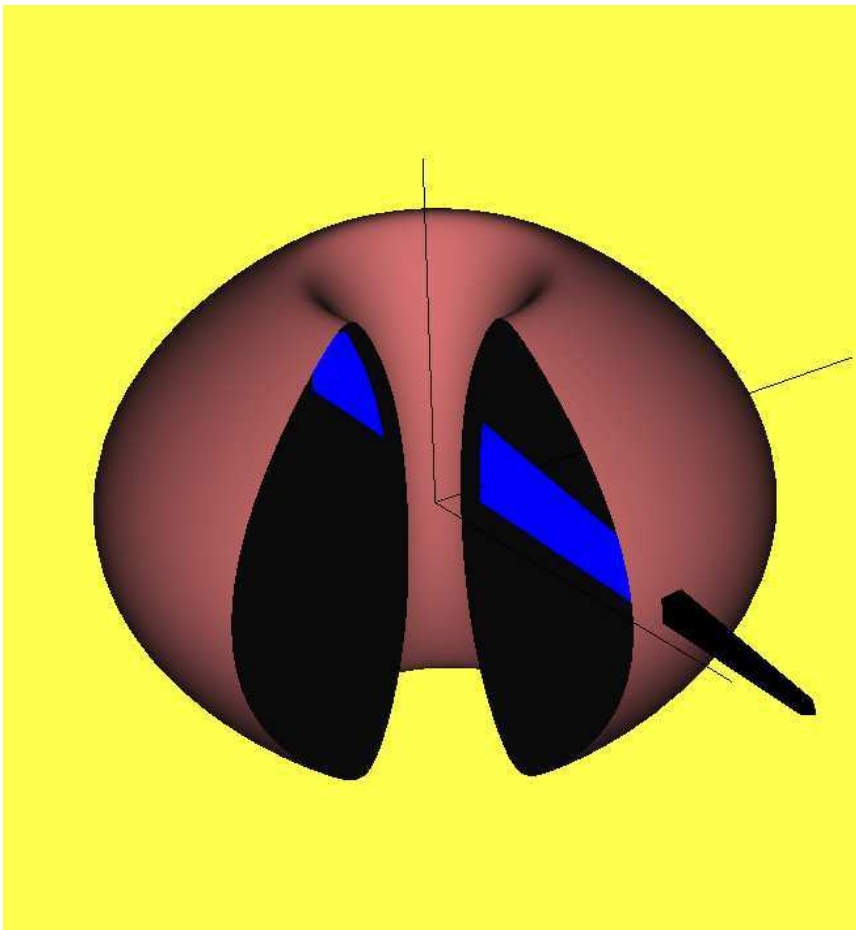
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2 Basics of Lithium Wall Fusion

What will happen if: (a) Neutral Beam Injection (NBI) supplies particles into the plasma core, while (b) a layer of Lithium on the Plasma Facing Surface (PFC) absorbs all particles coming from the plasma ?

(Assume that maxwellization is much faster than the particle diffusion.)



Plasma temperature will be uniform

Plasma physics is not involved into this answer.

The reason is very simple:

with pumping walls there is no cold particles in the system (other than Maxwellian)

$$\nabla T_i = 0, \quad \nabla T_e = 0 \quad (2.1)$$

Ion/electron temperature gradient instabilities (ITG, ETG), which are the major cause of energy losses, will be eliminated automatically

The best possible confinement regime

In fact, any thermo-conduction will be eliminated

$$q_i = 0, \quad q_e = 0 \quad (2.2)$$

Energy from the plasma will be lost only due to particle diffusion

$$\frac{d}{dt} \int \frac{3}{2} n (T_i + T_e) dV \simeq \oint \left(\frac{5}{2} \Gamma_i T_i + \frac{5}{2} \Gamma_e T_e \right) dS \quad (2.3)$$

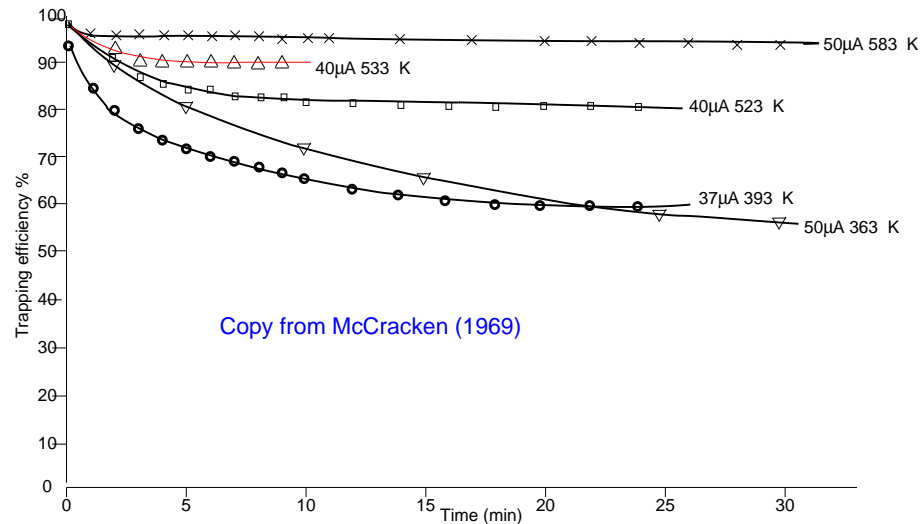
Unlike thermo-conduction, the particle diffusion is determined by the best confined component.

$$\Gamma_i = \Gamma_e \quad (2.4)$$

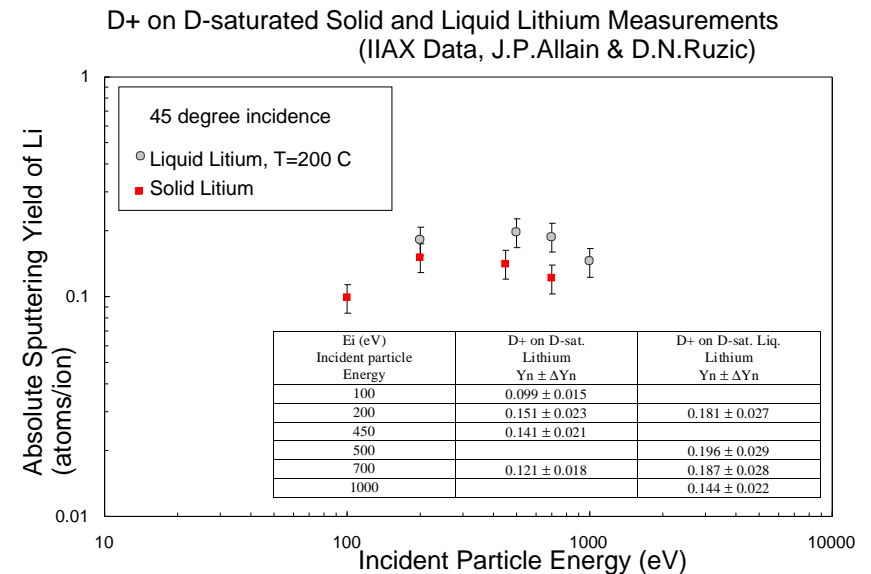
**For the first time the theory revealed the regime which
is not sensitive to anomalous electrons**

Li is an outstanding pump for H,D,T

Lithium can retain $\simeq 10\%$ of H,D,T atoms per Li atoms



McCracken retention curves



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Plasma-material interaction Group

Because of evaporation, the surface temperature of Li should be limited (by $\simeq 400^\circ$ C)

Probably, the short lasting retention allows higher temperatures (R.Majeski)

More Li technology studies are necessary

$V \simeq 1$ cm/sec is sufficient for pumping

PLD \equiv actively cooled plates with flowing $h \simeq 0.1$ mm Li layer

Gravity, Marangoni effect, residual $\mathbf{j} \times \mathbf{B}$ forces,

$$V_g = \frac{\rho g h^2}{2\nu} \sin \theta = 0.049 \sin \theta \text{ [m/s]},$$

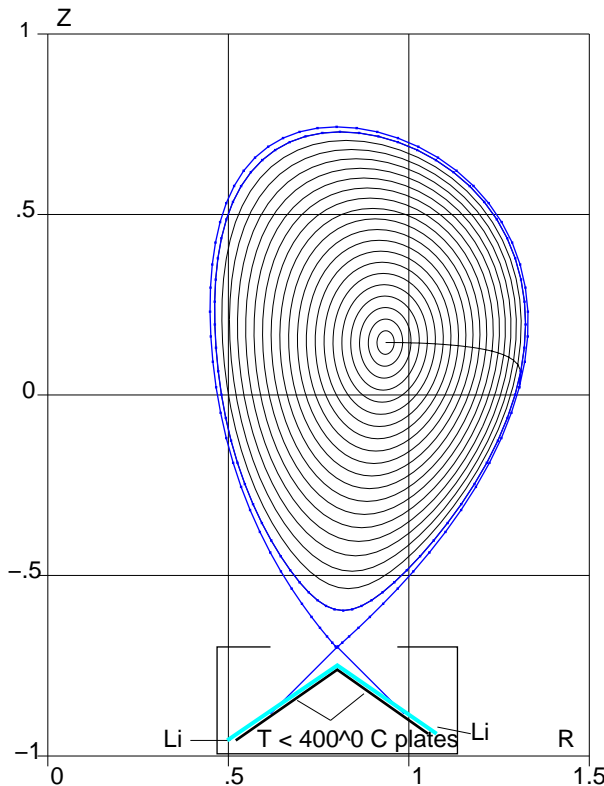
$$V_M = \frac{d\sigma(T)}{dT} \frac{h \nabla T}{\nu} = 0.8 h \nabla T \text{ [m/s]} \quad (2.5)$$

are sufficient for replenishing Li surface.

Lithium can accept 5-10 MW/m² and keep $T_{Li} < 400^\circ\text{C}$

$$\chi_{Li} = 47.6,$$

$$\Delta T [^\circ\text{C}] = 100 \frac{q}{4.7} \cdot h \left[\frac{\text{MW}}{\text{m}^2} \cdot \text{mm} \right]. \quad (2.6)$$

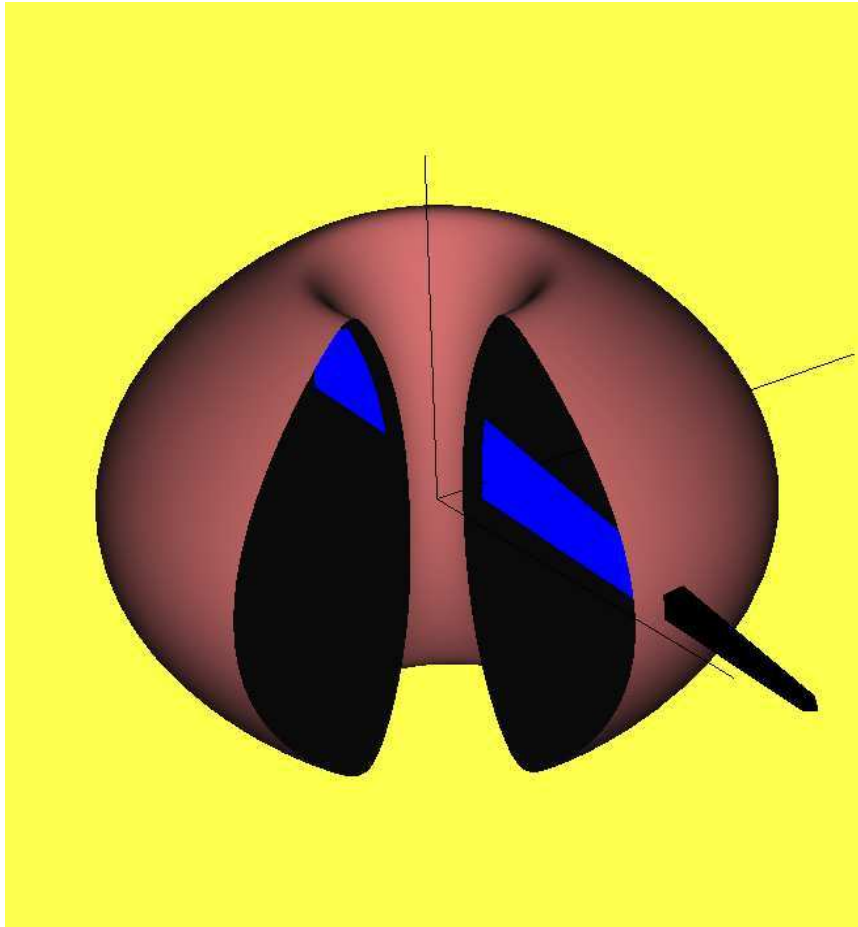


Power extraction is limited by the coolant temperature, rather than by the temperature of plasma facing surface.

No Li rivers, Li water-falls, evaporation, Li dust, pellets, LiLi trays, meshes, sponges, or thick (≥ 1 mm) Li on the target plate

Fueling does not represent the issue

NBI is a ready-to-go fueling method for LiWF



The energy should be consistent with the plasma temperature

$$E_{NBI} = \left(\frac{3}{2} + 1 \right) (T_i + T_e),$$

e.g., for

$$T_e \simeq T_i \simeq 16 \text{ keV}$$

$$E_{NBI} = 80 \text{ keV}$$

In absence of cold particles from the walls, after collisional relaxation

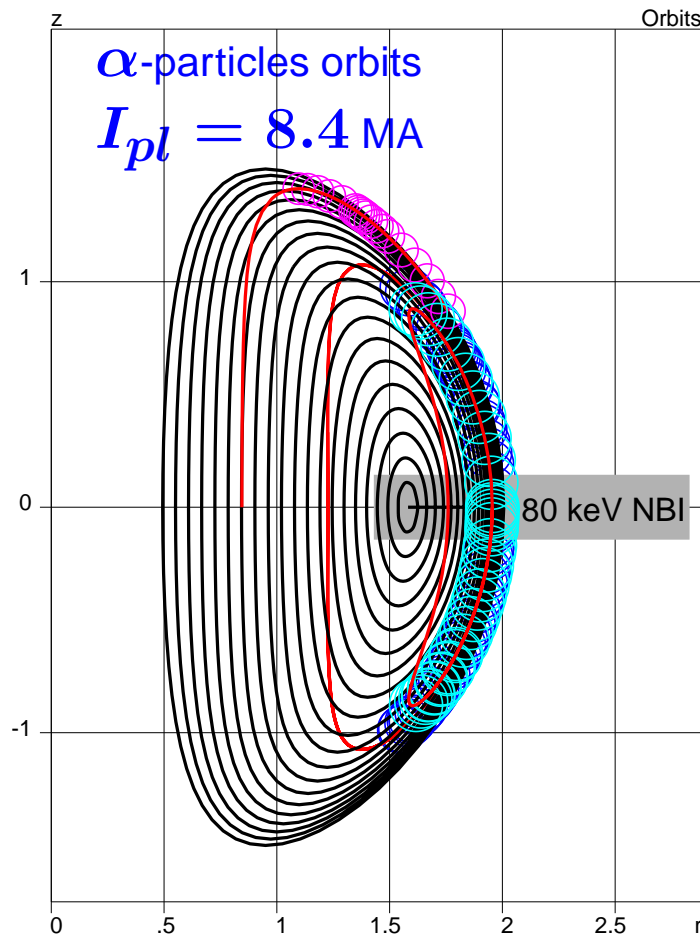
$$\nu_i = 68 \frac{n_{20}}{T_{i,10}^{3/2}}, \quad \nu_e = 5800 \frac{n_{20}}{T_{e,10}^{3/2}}$$

the temperature profile becomes flat automatically

$$T_i = \text{const}, \quad T_e = \text{const}, \quad T_e < T_i$$

**The plasma is always in the “hot-ion” regime
(as all existing machines)**

With high τ_E alphas can be lost



Large Shafranov shift in STs makes core fueling possible

The charge-exchange penetration length at $E = 80$ keV

$$\lambda_{cx} \simeq \frac{0.6}{n_{e,20}} [m]$$

The distance between magnetic axis and the plasma surface in projected RDF

$$R_e - R_0 = 0.3 - 0.5 [m]$$

80 keV NBI can provide core fueling and control of fusion power

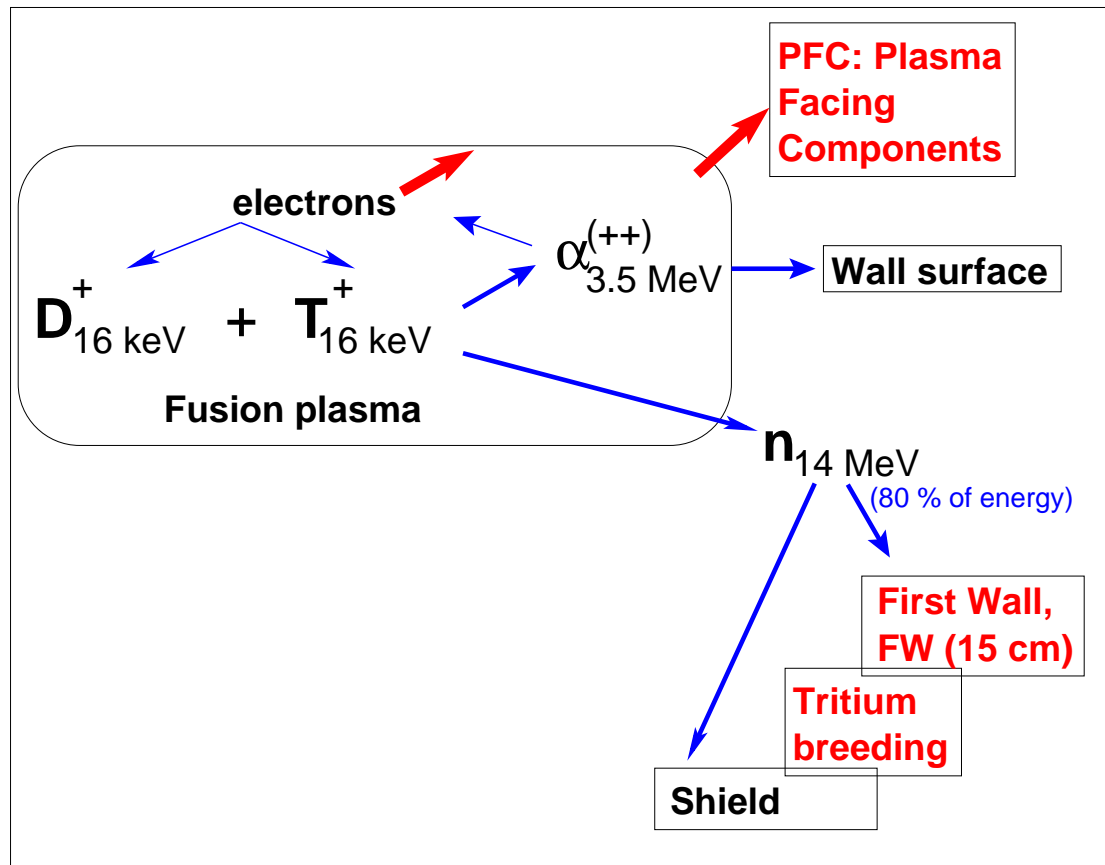
Even at 8.4 MA 60 % of alphas can be intercepted at first orbits (e.g. by Li jets)

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3 Two concepts: BBBL70 and LiWF

“The Bib_ble of the 70s” (BBBL70) relies on plasma heating by alpha-particles



Flow pattern of fusion energy (since the 50s)

Ignition criterion:

$$f_{pk} \cdot \langle p \rangle \cdot \tau_E^* = 1$$

[MPa · sec]

Peaking factor f_{pk} :

$$f_{pk} \equiv \frac{\langle 16p_D p_T \rangle}{\langle p \rangle^2}$$

Plasma pressure p :

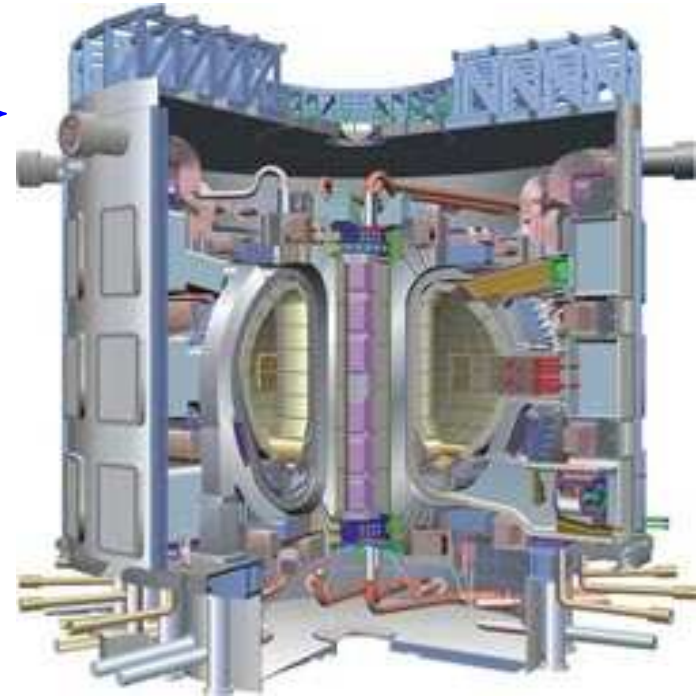
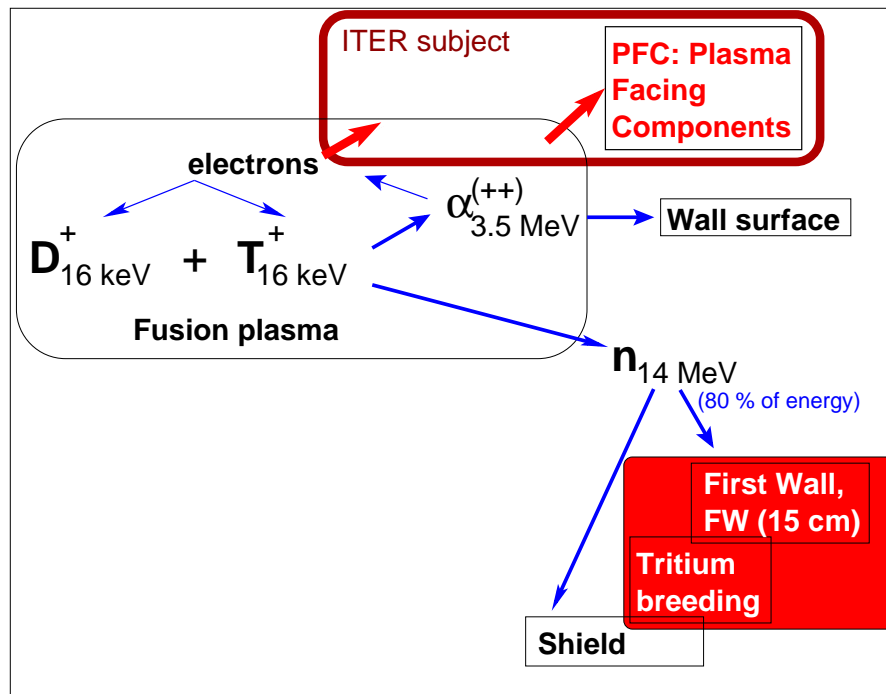
$$p = p_D + p_T + p_e + p_\alpha + p_I,$$

$$p_e > p_D + p_T$$

The plasma is in the “hot-electron” regime, the worst one.

ITER targets the alpha-heating regime

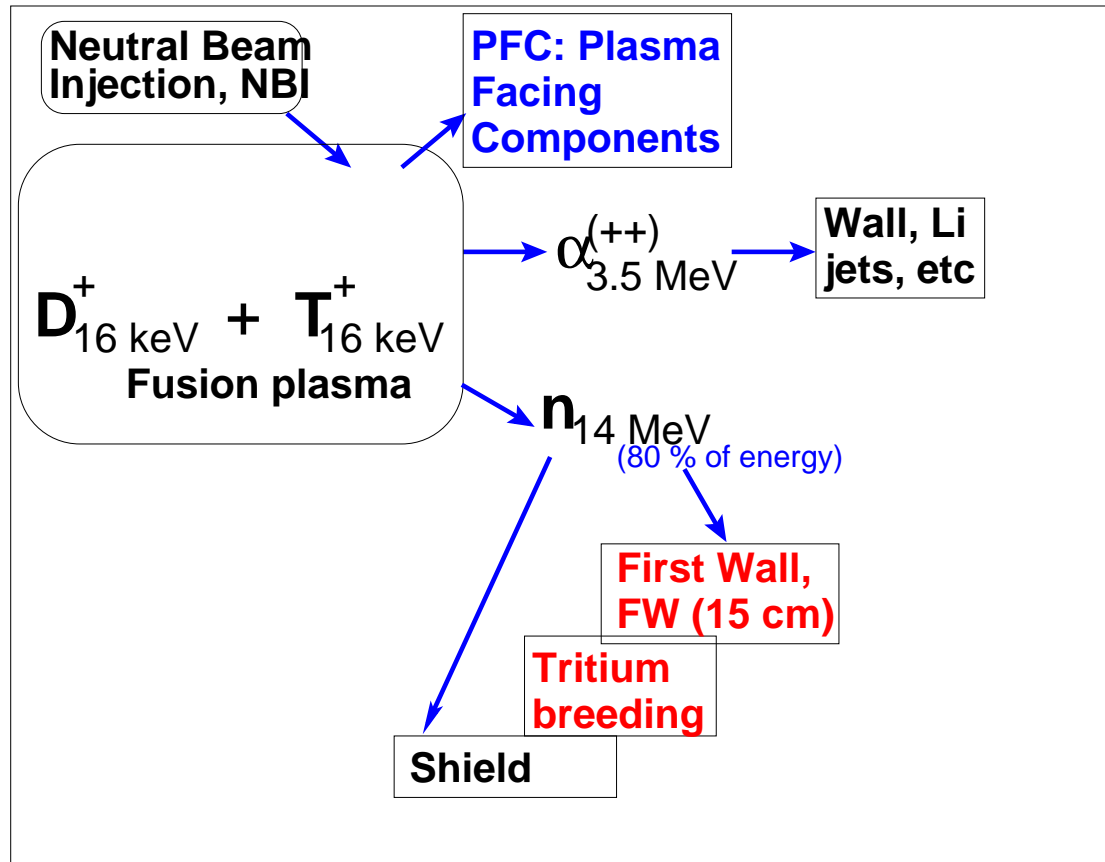
All current plasma physics issues are passed unresolved to the ITER “burning plasma”



Being an implementation of the old concept, ITER only barely touches the reactor aspects of fusion

LiWF has a clean path to reactor

Reactor issues rather than plasma physics are the focus of LiWF



α -particles are free to go out of plasma

NBI controls both the temperature and the density

$$P_{NBI} = \frac{3 \langle p \rangle V_{pl}}{2 \tau_E},$$

$$\frac{dN_{NBI}}{dt} = \Gamma_{core \rightarrow edge}^{ions}$$

Super-Critical Ignition (SCI) confinement is necessary to make NBI work this way

$$\tau_E \gg \tau_E^*$$

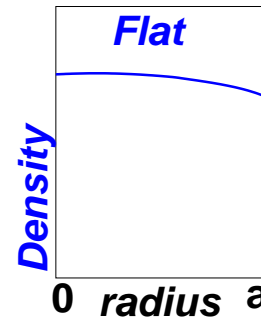
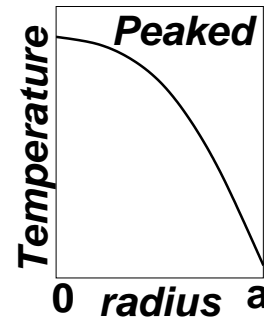
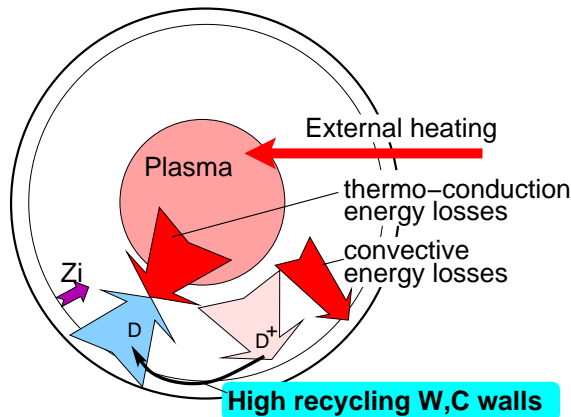
LiWall concept has a clean pattern of flow of fusion energy

**LiWF conceptually resolves fundamental issues,
intractable for BBBL70 for 40 years**

Right plasma-wall contact is the key

BBBL70 uses the science for keeping alive a failed concept

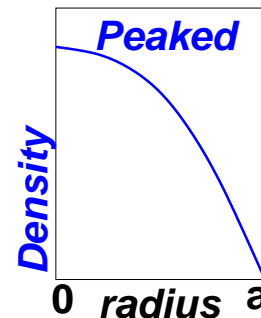
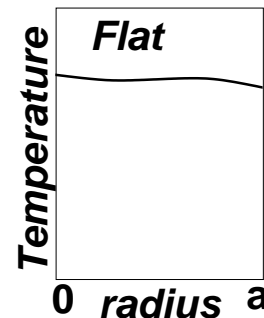
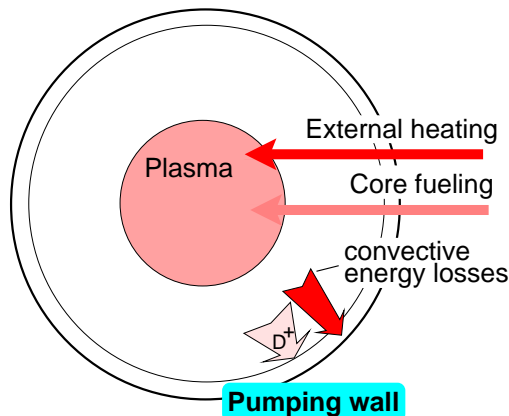
BBBL70 requires a low temperature plasma edge



As a "gift" from plasma physics BBBL70 gets ITG/ETG turbulent transport.

Bad core and edge stability (sawteeth, ballooning modes, ELMs)

Most of the plasma volume does not produce fusion



In LiWF the high edge T is OK

No "gifts" from plasma physics (ITG/ETG, sawteeth, ELMs) are expected or accepted.

Stability is excellent. LiWF relies only on external control.

The entire plasma volume produces fusion

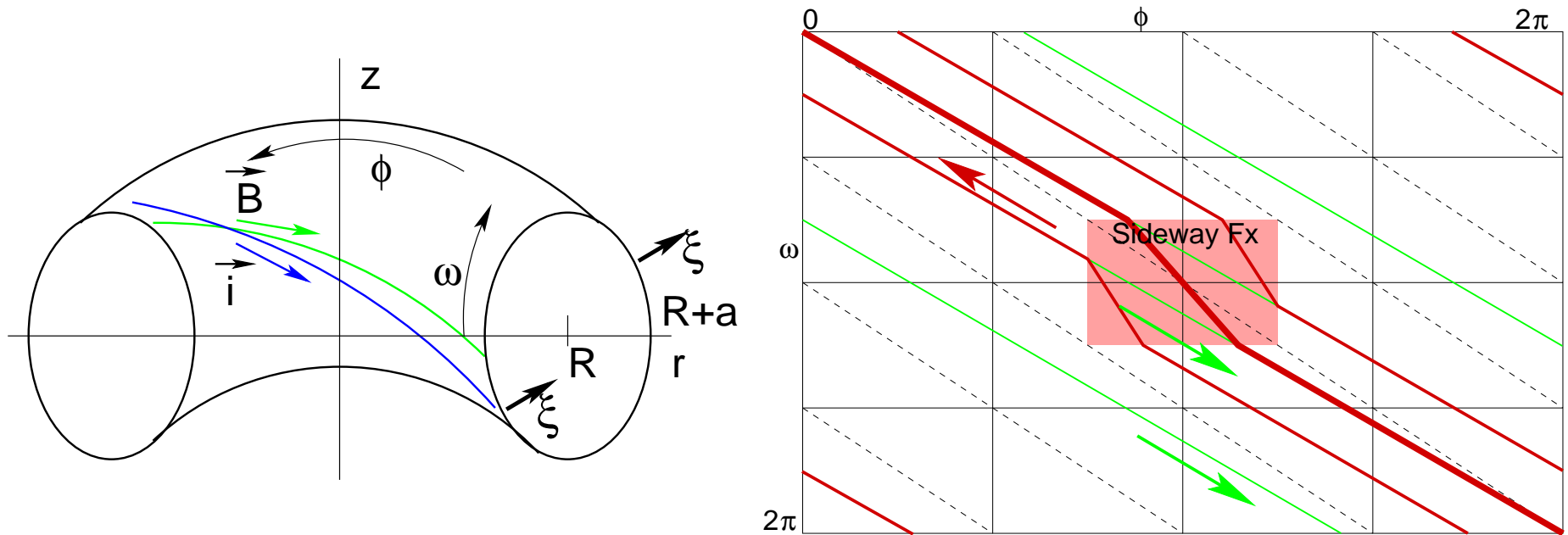
LiWF relies on science for making its concept consistent with the strategy of DT fusion

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4 LiWF contribution to science

55 year old MHD theory ignored the electric plasma-wall contact



Plasma-wall interaction is not an ignorable “kitchen effect”

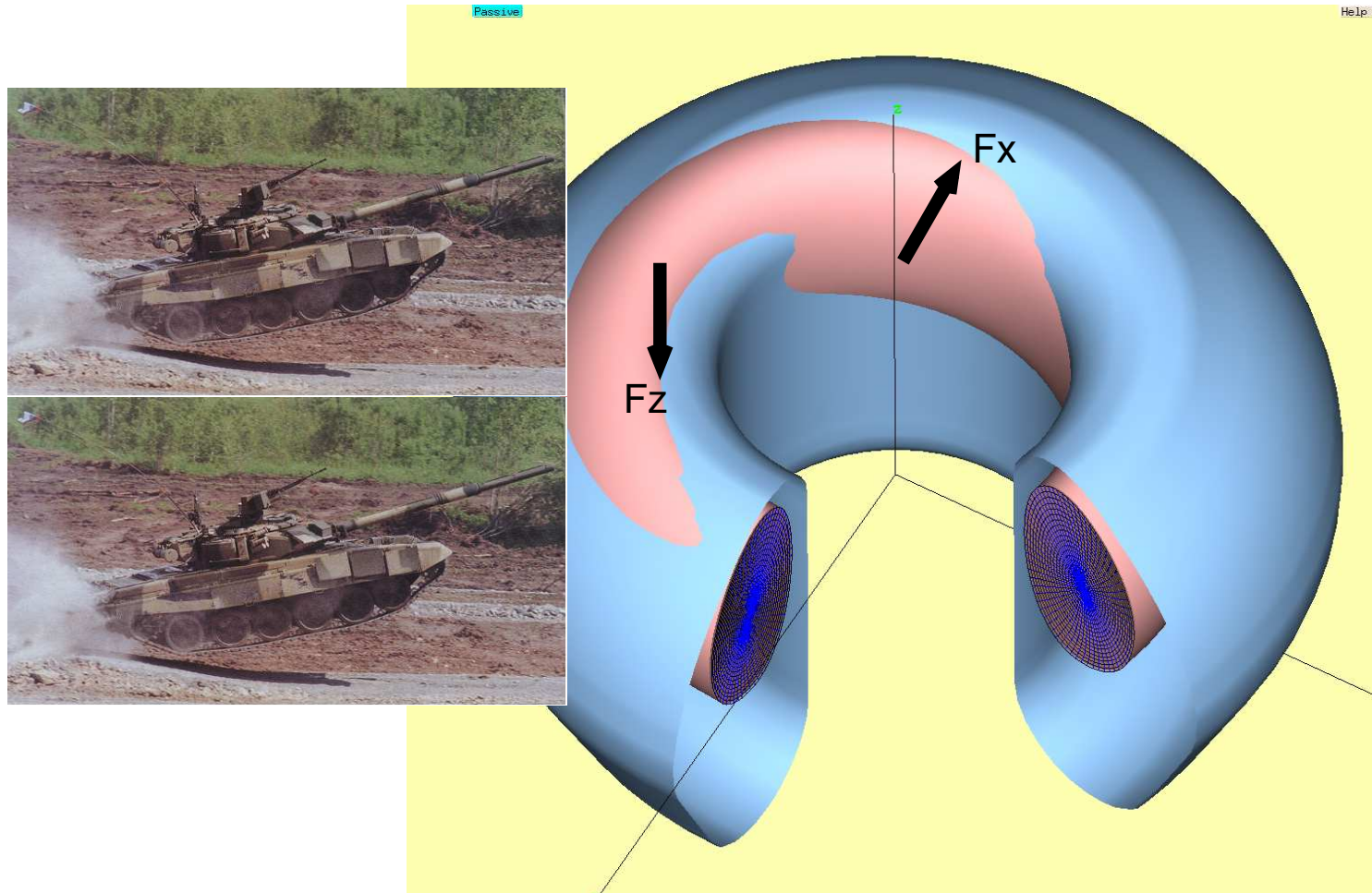
The current sharing between the plasma and the wall redistributes the forces (otherwise stabilizing) between the plasma surface and conducting structures and makes plasma unstable.

The current sharing affects the MHD stability in a fundamental way

The “Wall Touching Kink Modes” are always unstable.

WTKM $m/n=1/1$ during the disruptions

The impulse $\simeq 2MN \cdot \text{sec}$ of the sideways force to the ITER VV is equivalent to the hit by two 50 tonne tanks T-90S at the speed of 70 km/hour.



The sideways forces are just one thing which was missed by MHD in designing the next step devices

Scrape Off Layer Currents

Edge plasma is always in electric contact with the plasma facing components

SOL current and MHD activity in DIII-D

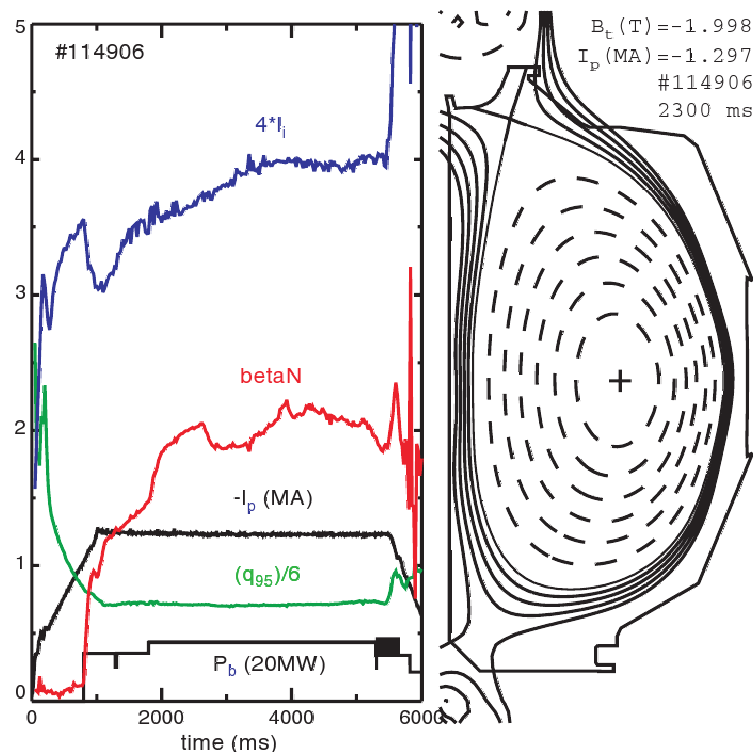


Figure 3. Pictorial discharge summary; the left-hand panel shows I_p in units of megaamperes, P_b in units of 20 MW, q_{95} divided by 6, β_N , and the nominal no-wall limit (here, 4 li). The right-hand panel shows the plasma boundary and four exterior flux surfaces in the SOL in solid lines, and interior flux surfaces in dashed lines. The exterior surfaces pass through points 1, 2, 3, and 4 cm away from the

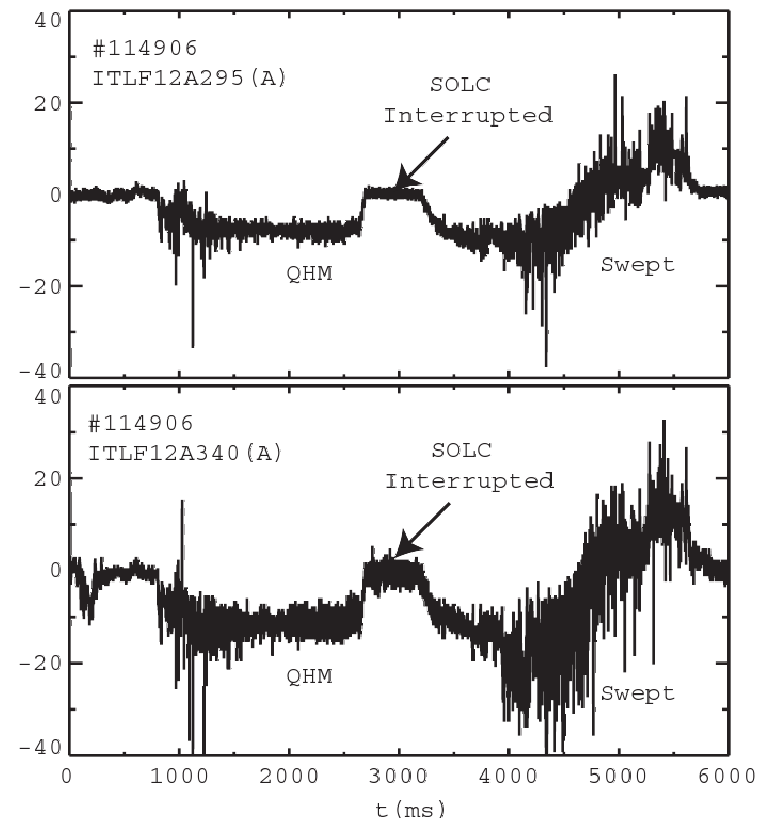


Figure 4. Signals from tile current sensors in tile ring #12 A in the discharge shown in the previous figure. It has a period of QHM over 1550–3800 ms. The upper outboard strike point is 'swept' over 3200–4000 ms. Discharge time: 12700–2200 ms.

Hiro Takahashi and Eric Fredrickson (NF,2004) have found a link between SOLC and MHD on DIII-D

Takahashi Kink Modes

The current sharing effect can be included into MHD formalism

$$W_{TKM} \equiv \underbrace{W_{MHD}}_{\text{conventional}} + \underbrace{\frac{\lambda}{2} \int_{\text{wet-zone}} \vec{\xi}_n \cdot (\tilde{\mathbf{i}} \times \mathbf{B}) dS}_{\text{virtual work against the wet surface}}. \quad (4.1)$$

If the plasma test perturbation satisfies the equilibrium conditions, the W_{TKM} is reduced to

$$W_{TKM,eq} = \frac{1}{2} \int_{\text{plasma surface}}^* \vec{\xi}_n \cdot (\tilde{\mathbf{i}} \times \mathbf{B}) dS \rightarrow 0, \quad \tilde{\mathbf{i}} \parallel \mathbf{B}. \quad (4.2)$$

Surface currents $\tilde{\mathbf{i}}$, excited by the plasma perturbation and called “Hiro” currents (in contrast to “halo” currents), are closed through the wet-zone and make equilibrium possible.

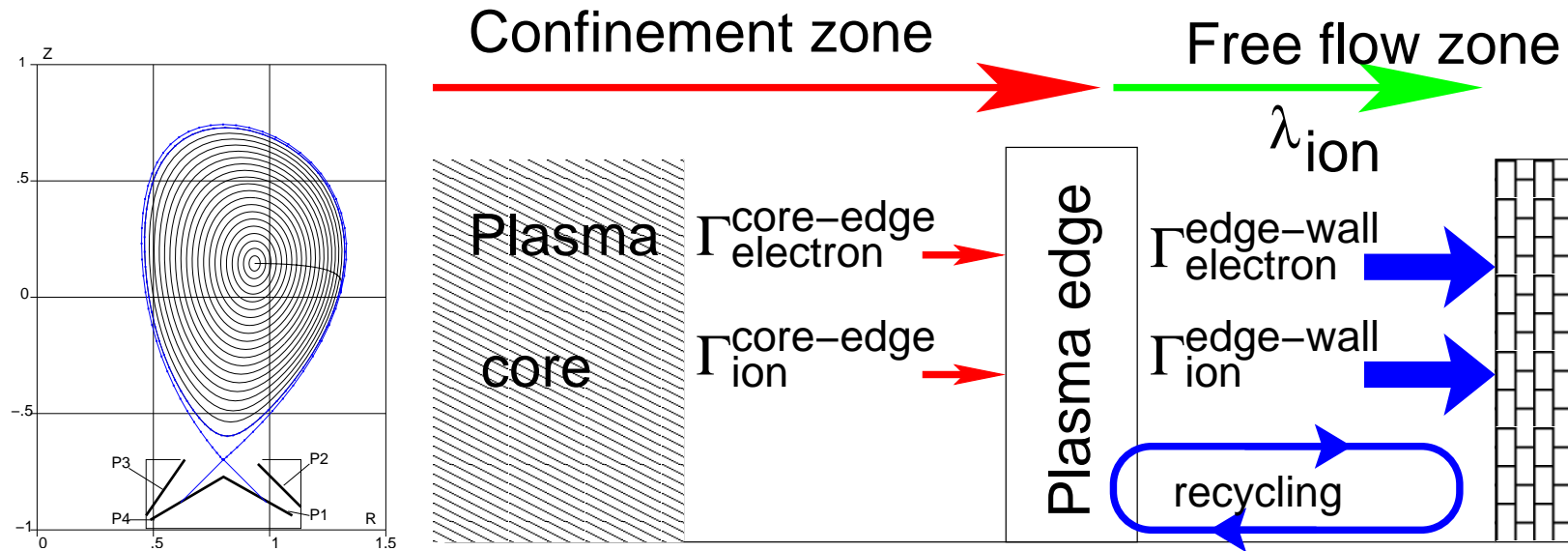
In MHD, the existence of a marginally stable perturbation is equivalent to the ideal instability, which I called “Takahashi Kink Modes” (TKM)

TKM are always IDEALLY unstable. Plasma edge density and recycling are the key factors for their behavior.

Without TKM, the existing boundary physics is highly incomplete.

New understanding of the plasma edge

LiWF requires recycling coefficient $R_{e,i} \ll 1$



Lithium PFC satisfies, at the very least, the condition of low recycling, $R_i \ll 1$

The importance of the secondary electron emission is not yet known. The scales

$$\rho_e^{se} = \frac{4.76}{B_T} \ll \rho_e^{SOL} = 238 \frac{\sqrt{T_{e,10keV}}}{B_T} \ll \rho_D = 14100 \frac{\sqrt{T_{i,10keV}}}{B_T} [\mu\text{m}] \quad (4.3)$$

give a chance to magnetic insulation (upon its necessity).

T_{edge} is a boundary condition

The edge plasma temperature is determined self-consistently by the particle fluxes (Krasheninnikov)

Across the last mean free path, λ_D , in front of PFC surface

$$\lambda_{D,m} = 121 \frac{T_{keV}^2}{n_{20}} \quad (4.4)$$

the energy is carried out by the moving particles

$$\frac{5}{2} \Gamma_{\text{electron}}^{\text{edge-wall}} T_e^{\text{edge}} = \int_V P_e dV, \quad \frac{5}{2} \Gamma_{\text{ion}}^{\text{edge-wall}} T_i^{\text{edge}} = \int_V P_i dV \quad (4.5)$$

The transport plasma properties near the edge do not affect T_{edge}

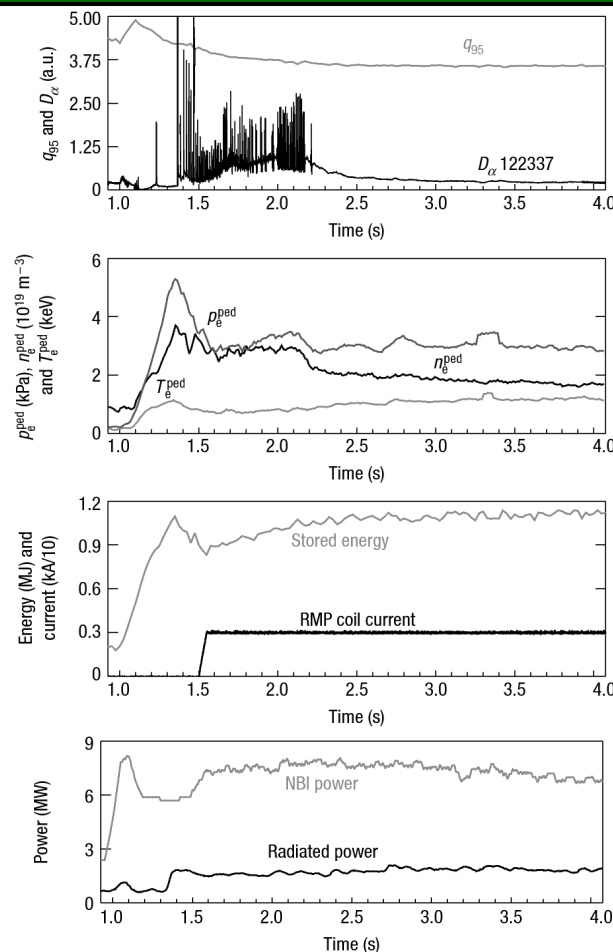
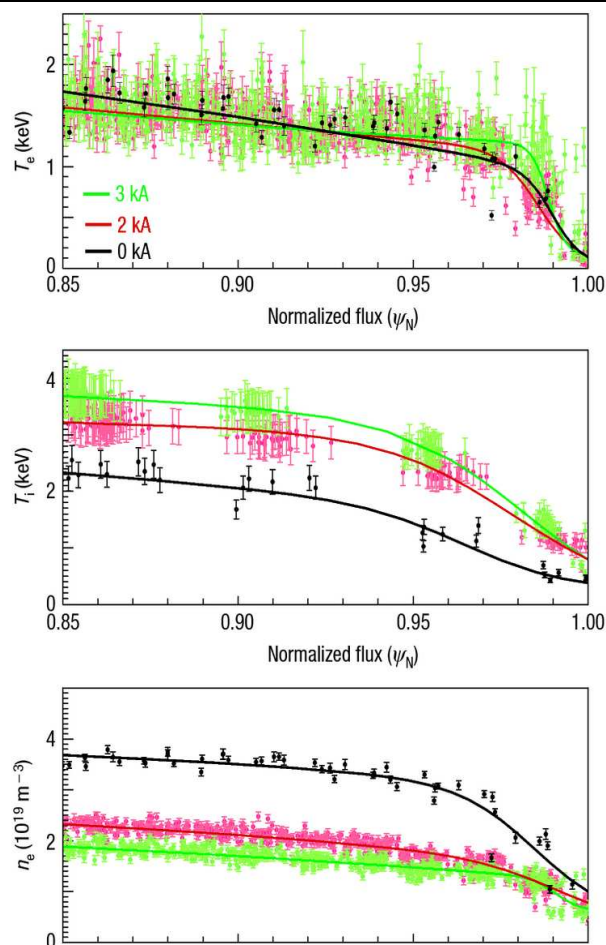
In LiWF

$$\Gamma_{\text{electron,ion}}^{\text{edge-wall}} \simeq \Gamma_{\text{electron,ion}}^{\text{core-edge}}, \quad \rightarrow T_{\text{edge}} \simeq T_{\text{core}}$$

For edge temperature $T_{e,i} \simeq 1 \text{ keV}$ (low collisionality H-mode) the mean free path λ_D is very long $\simeq \text{km's}$

DIII-D made crucial input to LiWF

Resonance Magnetic Perturbation experiments have confirmed our, LiWF, views. The plasma edge is at the temperature pedestal.



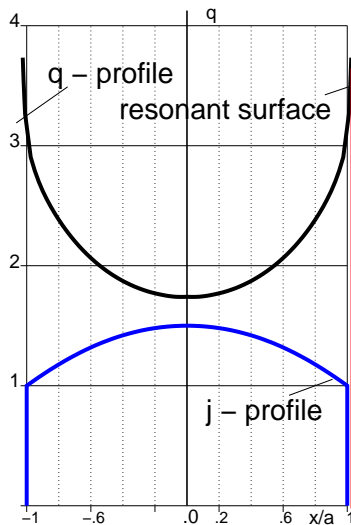
0 kA, 2 kA, 3 kA $I_{\text{RMP-coil}}$ T.Evans at al., Nature physics 2, p.419, (2006)

There is no confinement in the “edge transport barrier” zone

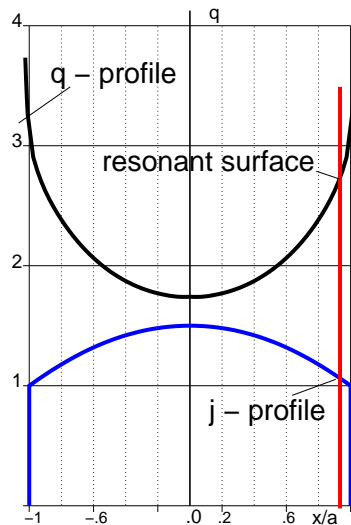
No ELMs, blobs in LiWF regime

A widespread belief in MHD theory is that the high edge current density is destabilizing (“peeling modes”)

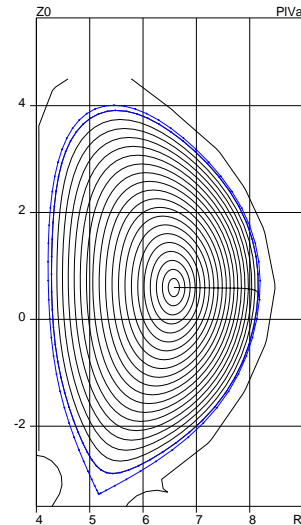
$$W \propto \int \frac{j' R \psi^2 d\rho}{B_{tor} \left(\frac{1}{q} - \frac{n}{m} \right)} \simeq \frac{j_{edge}}{B_{tor} \left(\frac{1}{q_{edge}} - \frac{n}{m} \right)} \psi^2$$



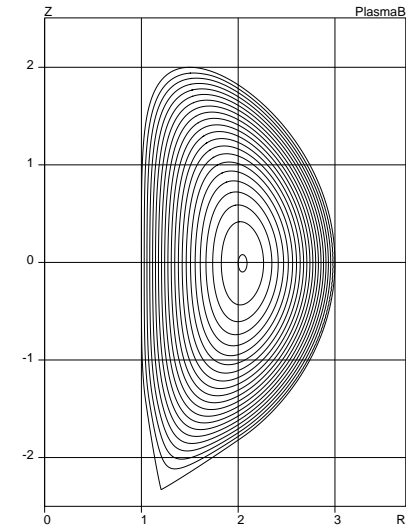
case 1: $m q_a < n$
Ideally unstable



case 2: $m q_a > n$
Tearing stable



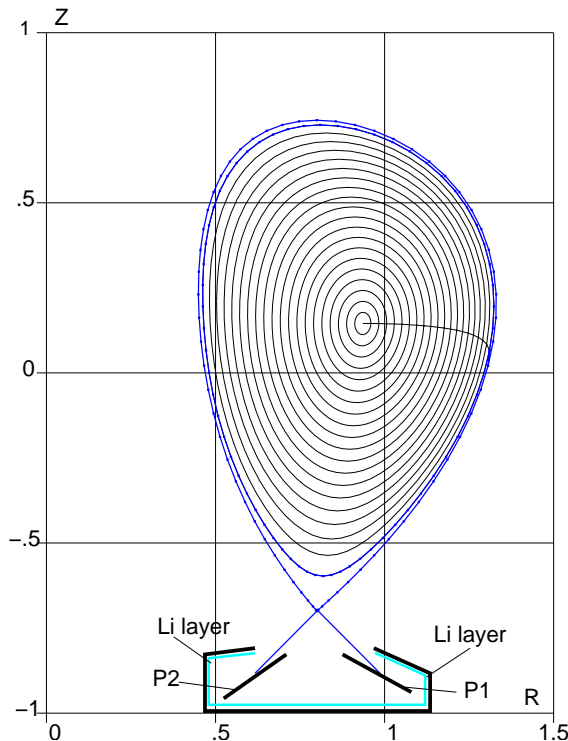
Ideally & tearing stable $j/B = \text{const}$ equilibrium, $j_{edge} \neq 0$



In presence of a separatrix, the finite edge current density is stabilizing as well as the low edge density. No ELMs, blobs, No Greenwald limit.

LiWF and stationary plasma

LiWF suggests a self-consistent approach to the stationary plasma



Three forces are acting on impurities on the way from PFC to the plasma:

1. A small electro-static force ZeE_{SOL} , directed back to the plate.
2. Friction $R_V \propto Z^2$ with the ion flow, also directed back to the plate.
3. **Thermo-force** $R_T \propto Z^2$, **driving impurities into the plasma.**

In addition, there is a direct plasma-wall interaction through the radial bursts of blobs.

At high T_{edge} the thermo-force is absent in the SOL,

leading to $Z_{eff} \simeq 1$

Interaction with the side walls is not expected (blobs are absent)

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5 R&D of LiWF

The LiWF concept has a solid scientific basis in both plasma theory and experiment.

Together with essentially existing technology and engineering LiWF is suitable for a Reactor Development Facility (RDF) as a necessary step toward a power reactor.

LiWF regime can be simulated in DD

No needs in alpha particles for heating.

Consistency with existing physics and technology simplifies the formulation of LiWF R&D

The LiWF is the only concept, which does not depend on anomalous behavior of electrons and associated mysteries

A simple Reference Transport Model (RTM) is relevant for projections of LiWall regime

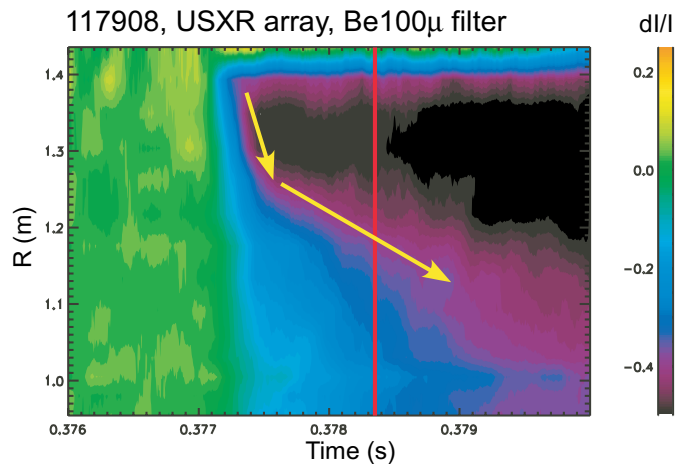
$$\begin{aligned}\Gamma^{core} &= \chi_i^{neo-classics} \nabla n \\ q_i &= \chi_i^{neo-classics} \nabla T_i, & \text{not important} \\ q_e &= \chi_i^{neo-classics} \nabla T_e, & \text{not important,}\end{aligned}$$

RTM predicts the feasibility of the super-critical ignition regime with $\tau_E \gg \tau_E^*$

RTM is consistent with NSTX, CDX-U

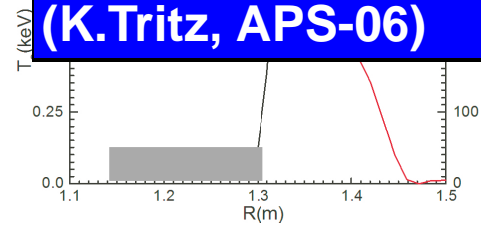
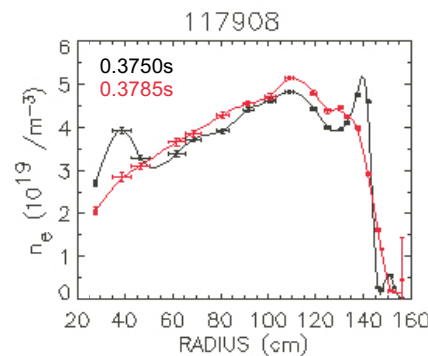
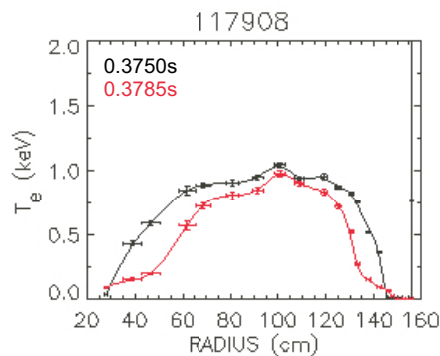


Perturbation Analysis Indicates Two Regions of $\chi_{e,pert}$



- T_e crash propagates from edge to core, n_e globally unperturbed
- Difference in propagation speed corresponds to differences in perturbation

NSTX experiments:
Ions are neo-classical,
Electron are anomalous,
Density profile is not "stiff"
(K.Tritz, APS-06)

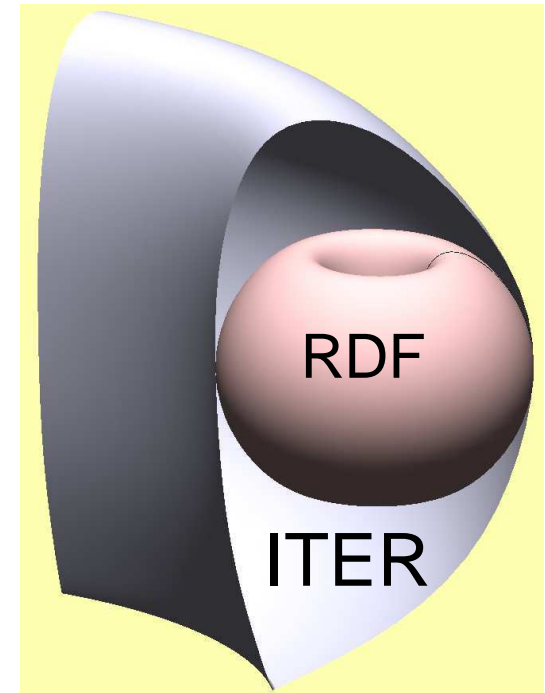
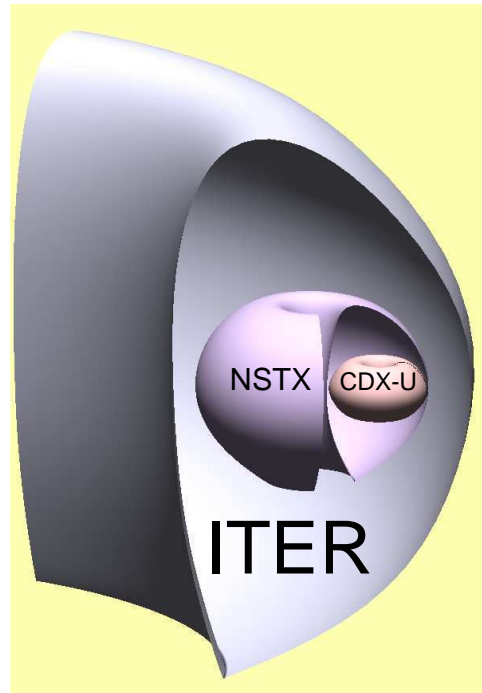
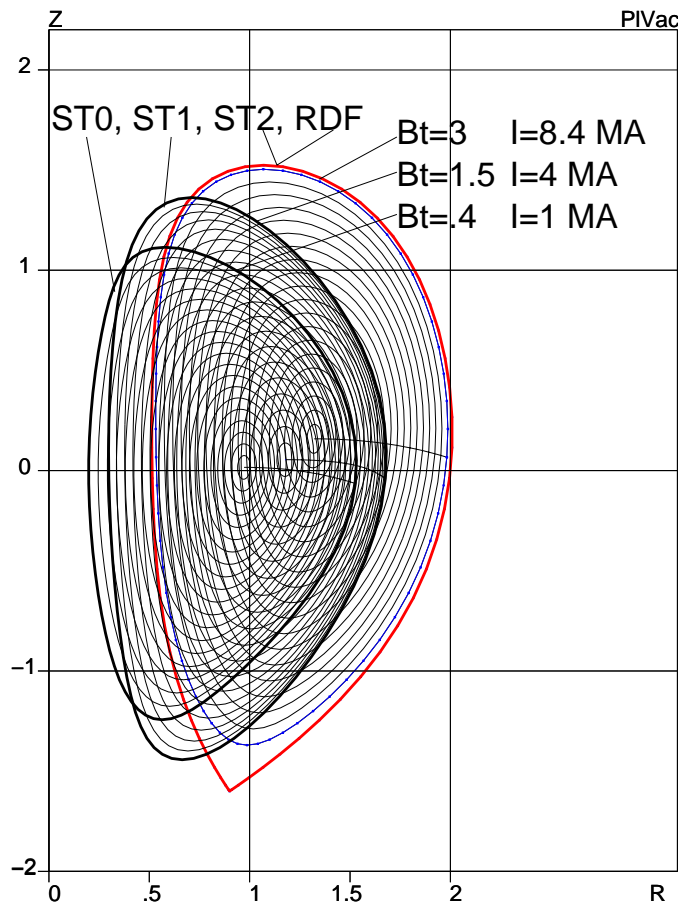


- Dependence of $\chi_{e,pert}$ on T_e gradient suggests critical gradient threshold

RTM reproduced the basic parameters of CDX-U discharges with Li tray.

New plasma regimes, not the size

Increase in performance of STs is provided by the increase in magnetic field and I_{pl}



RDF with $P_{DT} = 0.2 - 0.5$ GW is 27 times smaller than ITER

The program is very specific

3 steps of LiWF rely exclusively on the “present understanding of fusion” and existing technology. No big leaps.

Steps toward RDF	Milestone	Priorities and Mission
NSTX with molten LLTP (Li Loaded Target Plate), $B=0.4$ T, $I_{pl} = 1$ MA, $A=1.2$, $R_{outer} = 1.5$ m	Reproduce T11-M, CDX-U, FTU plasma pumping experiments	Plasma pumping. Low energy NBI. Stability. Clarify the system compatibility with molten Li
ST0 (modified NSTX) : $B=0.3-0.5$ T, $I_{pl}=0.7-1$ MA, $A=1.2$, $R_{outer} = 1.5$ m. LTX (modified CDX-U) $B=0.3$ T, $I_{pl}=0.3$ MA, $A=1.6$, $R_{outer} \simeq 1.65$ m.	Achieve RTM-like confinement: $\tau_E \rightarrow 2 - 3 \times \tau_{E,NSTX}$.	Plasma boundary. Stability. Start-up. Core fueling by low energy NBI. Collisionless SOL/PFC interaction. Role of C-walls. Creating a design concept of LPD for ST1.
ST1 : $B=1.5$ T, $I_{pl}=2-4$ MA, $A \simeq 5/3$, $\beta = 0.2 - 0.3$, $R_{outer} = 1.65$ m	Achieve Super-critical regime: $Q_{DT}^{equiv} > 5$, $f_{pk}P\tau_E > 1$	Plasma boundary. Stability. Physics and technology of LPD. Secondary electron emission. Role of TEM. Creating concept of a Startup and stationary LPD
ST2 : DD-prototype of ST3, $B=3$ T, $I_{pl}=4-8$ MA, $A \simeq 5/3$, $\beta = 0.3 - 0.4$, $R_{outer} = 2$ m, $Vol_{plasma} \simeq 30$ m ³	Achieve RDF stationary regime: $Q_{DT}^{equiv} = 30 - 50$	High $\beta \simeq 30 - 40$ %. Noninductive current drive. Integrate the stationary plasma regime for RDF. Assess the feasibility of DD fusion.
ST3 : DT neutron source. $B=3$ T, $I_{pl}=4-8$ MA, $A \simeq 5/3$, $R_{outer} = 2$ m, $Vol_{plasma} \simeq 30$ m ³	Achieve DT-stationary regime: $Q_{DT} = 30 - 50$, $P_{DT} = 0.2 - 0.5$ GW	Power extraction from α -particles, He exhaust. Integrate the stationary neutron producing regime for RDF mission.

The success of ST0 in the RDF program would bootstrap the necessary funding of fusion

LiWF vs BBBL70

LiWF is consistent with common sense in all reactor issues

Issue	LiWF	BBBL70 concept of “fusion”
The target	RDF as a useful tool	Political “burning” plasma
Operational point: Hot- α , 3.5 MeV Cold He ash $P_\alpha = 1/5 P_{DT}$ Power extraction from SOL Plasma heating	$P_{NBI} = E/\tau_E$ ”let them go as they want” residual, flashed out by core fueling goes to walls, Li jets conventional technology for $\frac{\tau_E^*}{\tau_E} P_\alpha$ ”hot-ion” mode: $NBI \rightarrow i \rightarrow e$	ignition criterion $f_{pk} p \tau_E = 1$ ”confine them” ”politely expect it to disappear” dumped to SOL no idea except to radiate 90 % of P_α by impurities first heat useless electrons: $\alpha \rightarrow e \rightarrow i$
Use of plasma volume	100 %	25-30 %
Tritium control	pumping by Li	tritium in all channels and in dust
Tritium burn-up	>10%	fundamentally limited to 2-3 %
Plasma contamination	eliminates the Z^2 thermo-force, clean plasma by core fueling	invites all “junk” from the walls to the plasma core
He pumping	Li jets, as ionized gas, $p_{in} < p_{out}$	gas dynamic, $p_{in} > p_{out}$
Fusion producing β_{DT}	$\beta_{DT} > 0.5\beta$	diluted: $\beta_{DT} < 0.5\beta$

**As a reactor concept, the BBBL70 is not consistent
with common sense and science**

LiWF vs BBBL70 in plasma issues

LiWF has a robust plasma physics and technology basis. It contributes to present understanding of fusion in unique way

Issue	LiWF	BBBL70 concept of “fusion”
Physics: Confinement Anomalous electrons Transport database Sawteeth, IREs ELMs, $n_{Greenwald}$ -limit p'_{edge} control Fueling Fusion power control Operational DT regime	diffusive, $RTM \equiv \chi = \chi_e = D = \chi_i^{neo}$ play no role scalable by RTM (Reference Transp. Model) absent absent by RMP through n_{edge} existing NBI technology existing NBI technology identical to DD	turbulent thermo-conduction is in unbreakable 40 years old marriage with anomalies religious beliefs on applicability of scalings to “hot e”-mode unpredictable and inavoidable intrinsic for low T_{edge} through T_{edge} and reduced performance no clean idea yet no clean idea yet needs fusion DT power for its development
Time scale for RDF:	$\Delta t \simeq 15$ years	$\Delta t \simeq \infty$
Cost:	\simeq \$2-2.5 B for RDF program	\simeq \$20 B with no RDF strategy

3 step RDF program of LiWF suggests a way for bootstrapping its funding

With no tangible returns the BBBL70 is irrational and compromises credibility of fusion

Contents

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6 Summary.

LiWF is a separate, self-consistent magnetic fusion concept, rather than an “improvement” of the old one.

After 40 years since acceptance of tokamaks as a mainstream approach for magnetic fusion it is the time to switch into a reasonable reactor concept

**Ray Orbach and Sam Bodman give
us a unique chance to do this
in time**

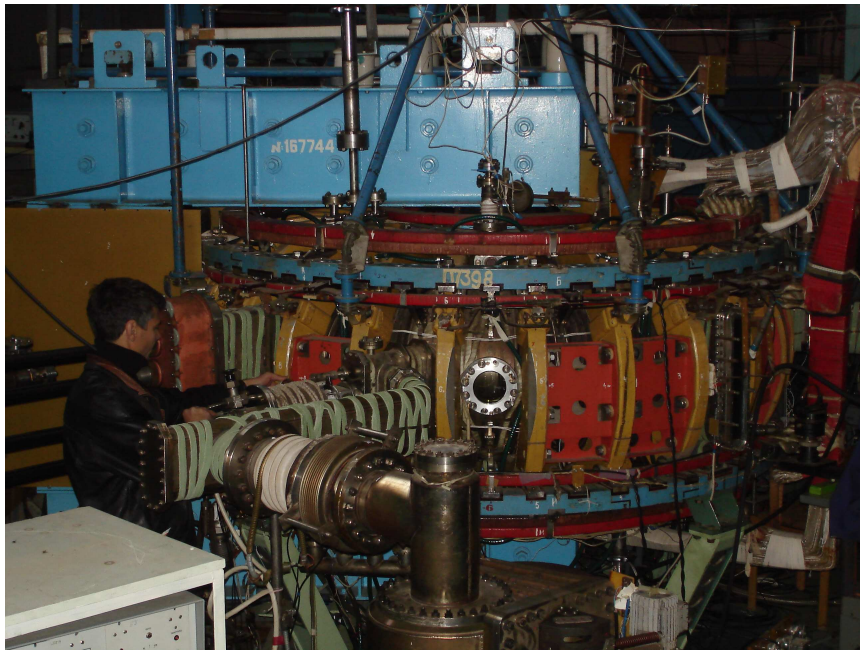
So far, there is no implementation of the pumping PFC surface together with core fusion.

At the same time with only one exception of ill-fated Dimes experiment on DIII-D, the effects of lithium conditioning on confinement, stability, radiation, Greenwald limit were exclusively positive.

**NSTX is the most ready device for making a conclusive
experiment**

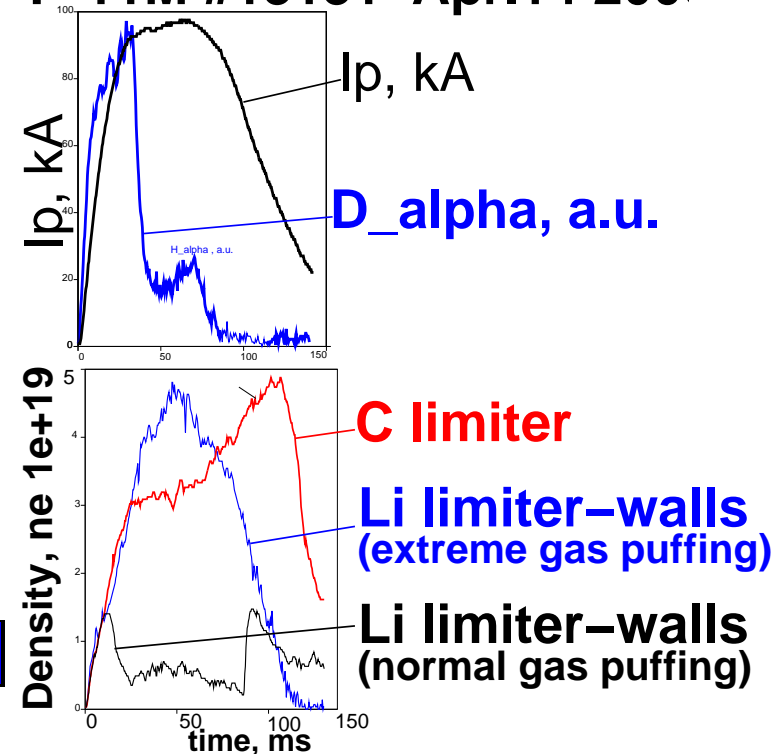
In 1998 T-11M tokamak (TRINITI, Troitsk, RF) demonstrated outstanding plasma pumping by Li coated walls

(<http://w3.pppl.gov/~zakharov/Mirnov010221/Mirnov.ppt>, p.18, *Exper. Seminar PPPL, Feb. 21, 2001*)



T11M and DoE's APEX/ALPS technology programs triggered the idea of LiWalls

T-11M #13131 Apr.14 2000



Lithium completely depleted the discharge in T-11M

In PPPL, CDX-U demonstrated similar pumping capabilities

Reference Transport Model (RTM) is natural for LiWall regime

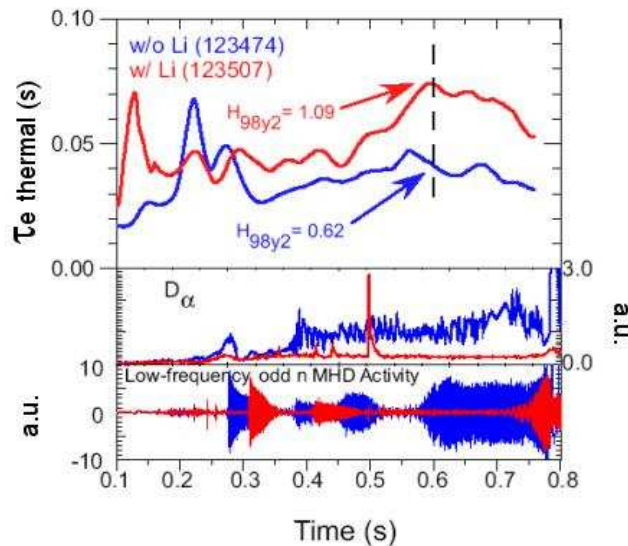
$$\begin{aligned}
 q_i &= \chi_i^{neo-classics} \nabla T_i, & \text{not important,} \\
 q_e &= \chi_i^{neo-classics} \nabla T_e, & \text{not important,} \\
 \Gamma_{i,e} &= \chi_i^{neo-classics} \nabla n
 \end{aligned}
 \tag{7.1}$$

Parameter	CDX-U	RTM	RTM-0.8	glf23	Comment	Table 1
\dot{N} , 10^{21} part/sec	1-2	.98	0.5	0.8-3	Gas puffing rate adjusted to match measured β_j	
β_j	0.160	0.151	0.150	0.145		
l_i	0.66	0.769	0.702	0.877	internal inductance	
V, Volt	0.5-0.6	0.77	0.53	0.85	Loop Voltage	
τ_E , msec	3.5-4.5	2.7	3.8	2.3		
$n_e(0)$, 10^{19} part/ m^3		0.9	0.7	0.9		
$T_e(0)$, keV		0.308	0.366	0.329		
$T_i(0)$, keV		0.031	0.029	0.028		

RTM does not contradict CDX-U measurements and equilibrium reconstruction

NSTX had 2 campaigns with Li conditioning by evaporation

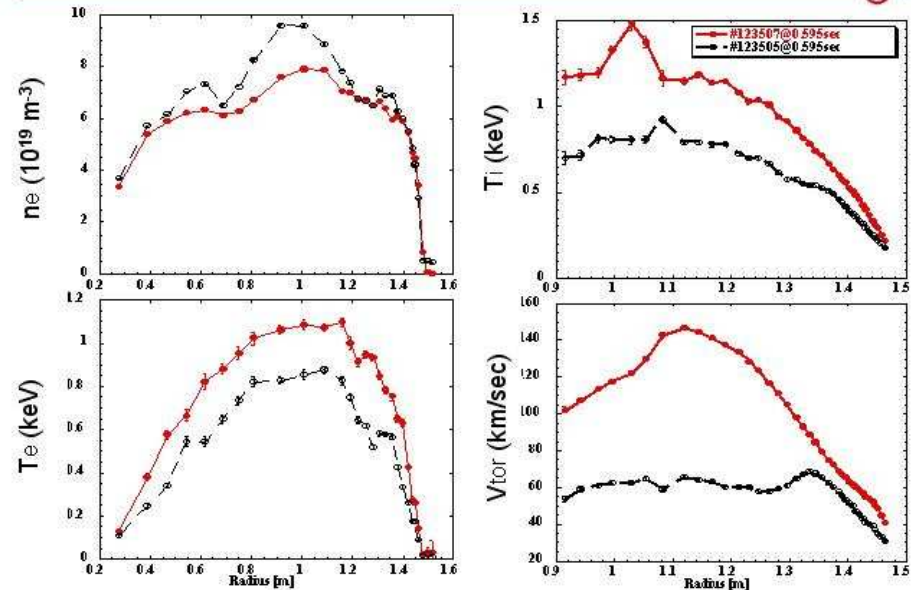
Lithium Evaporation Has Increased NSTX Confinement
Eliminated ELMS and Reduced MHD Activity - 2007



PPPL

2007 Transitional Profiles @ 0.6 sec
123505 No Li, Faint ELMS 123507 With Li, No ELMS

NSTX



PPPL

There are indications of improved confinement with Li conditioning on NSTX after evaporation.

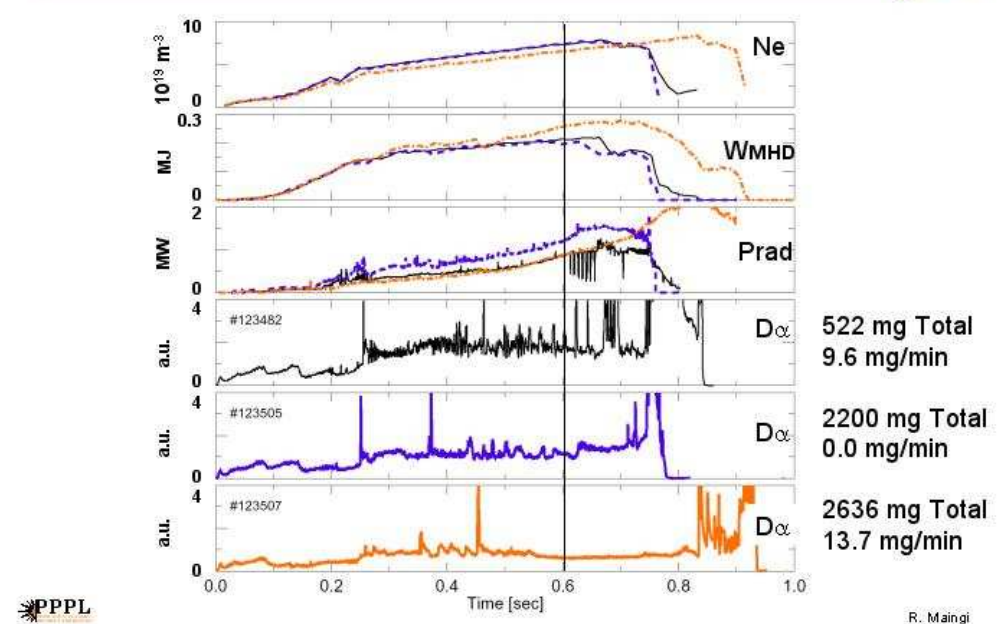
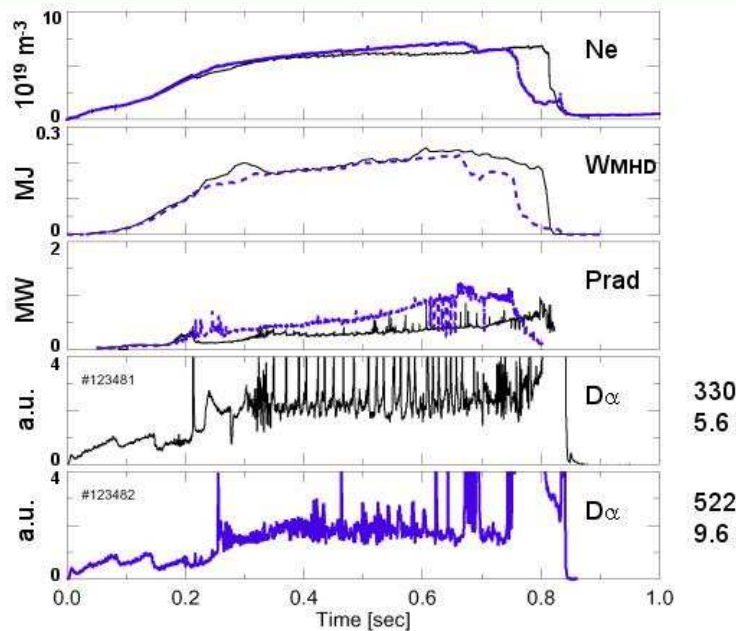
NSTX is not yet in the LiWall regime. There is no effect on the density rise

ELMs were suppressed after Li conditioning on NSTX

ELMS → Faint ELms → No ELMS Transition (I)

ELMS → Faint ELms → No ELMS Transition (II)

NSTX

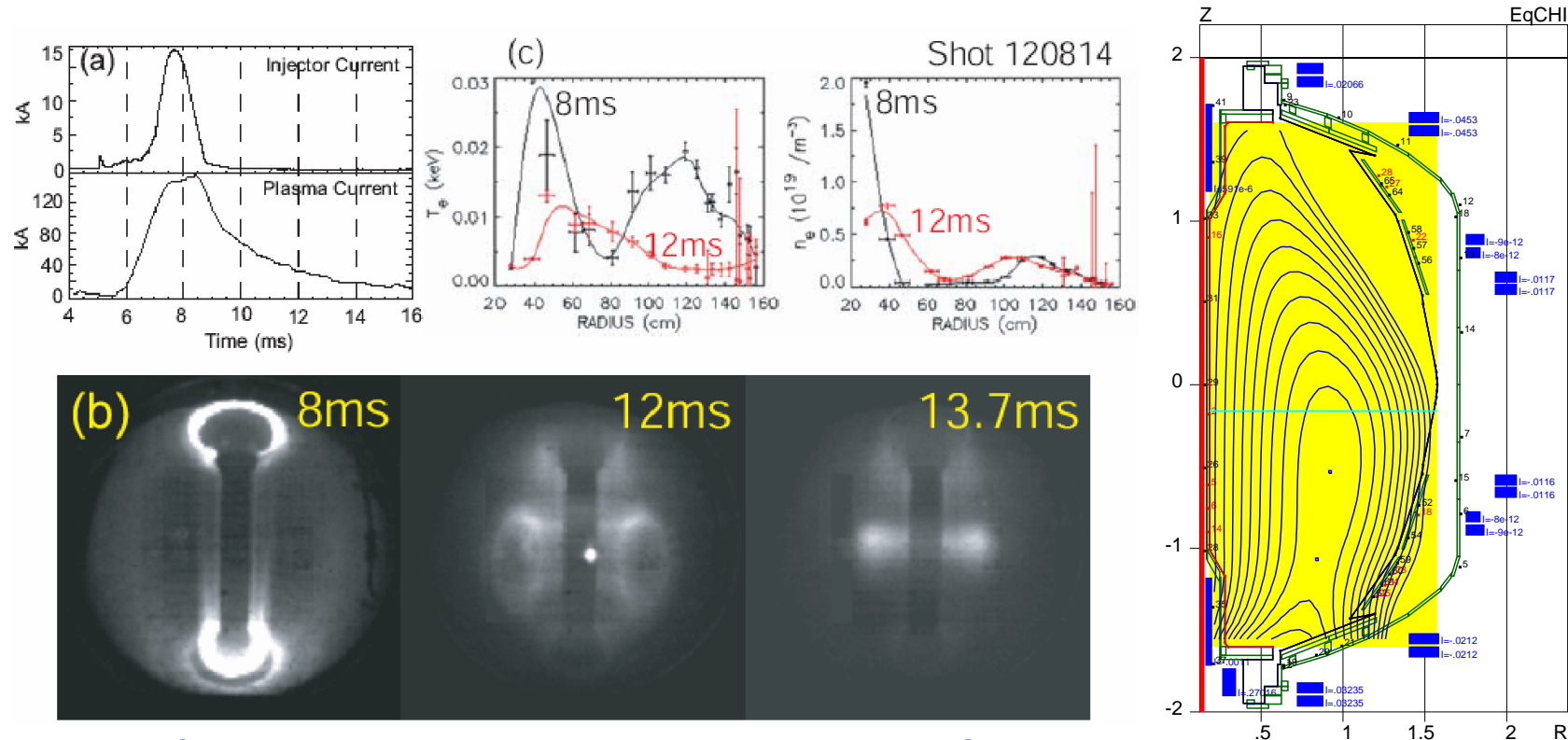


R. Maingi

Four shots are shown (D.Mansfield): before Li evaporation, after depositing $\simeq 200$ mg, then +1700 mg, and +400 mg.

**It was a surprise, although consistent with tendencies,
how easy ELMSs were suppressed**

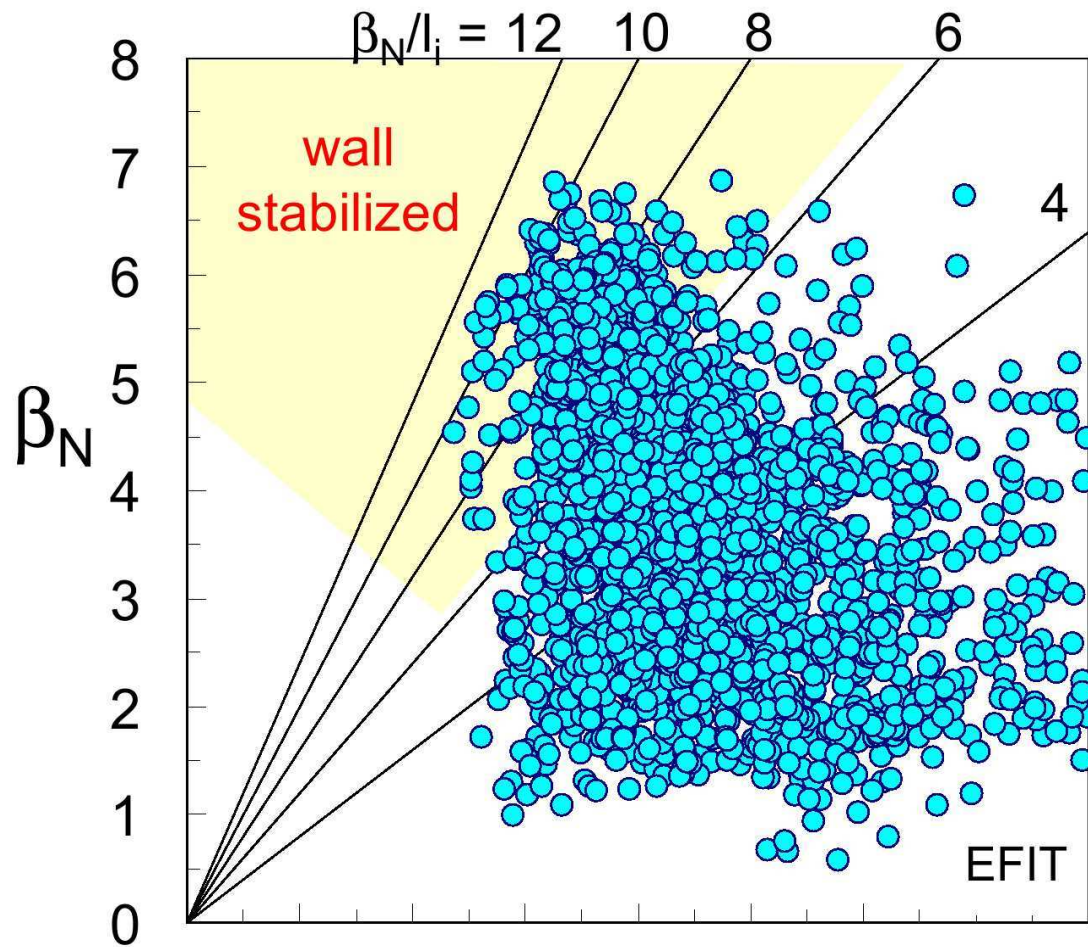
LiWF is compatible with both inductive and CHI start-up



In 2006 CHI startup generated 160 kA current in NSTX From
R.Raman et al., PPPL-4207 (2007)

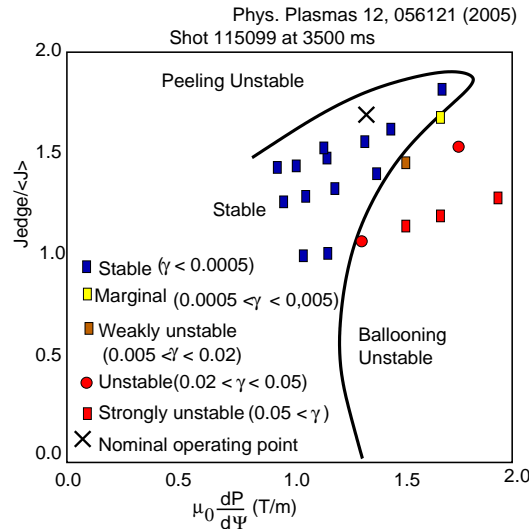
**With Li electrodes, even in the worst case scenario, CHI will create
 a perfect, transient Li plasma with $Z_{eff}=3$
 (typical for C-wall machines)**

The stability data base for RDF is already in a good shape

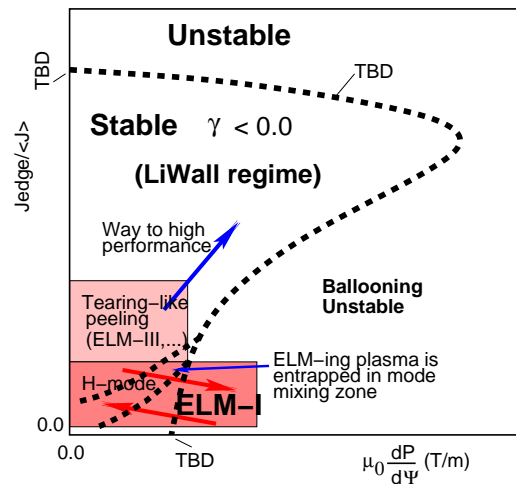


In 2004, beta in NSTX has approached the record level of 40 %

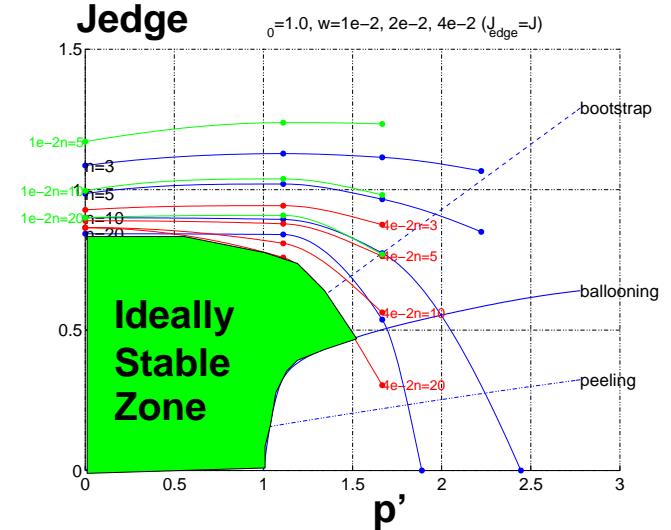
Peeling-ballooning diagram of Phyl Snyder initiated theory of ELMs



Peeling-ballooning diagram (P.Snyder)



"Heuristic diagram" (Zakharov, 2005)



Keldysh Institute calculation, (Medvedev, 2003)

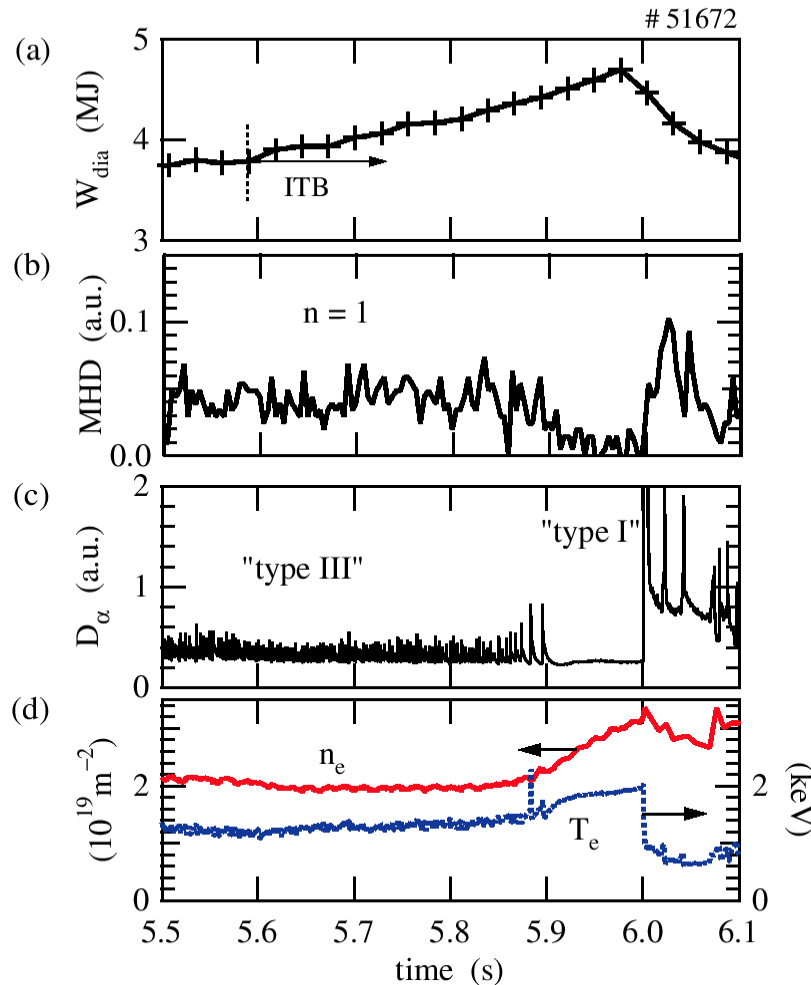
New understanding is that the finite current density at separatrix is stabilizing for ELMs, while pressure remains destabilizing.

1-D energy principle is now written to check a single point $p = 0, j_{edge} \neq 0$

$$W = \oint \oint \psi(l) i_{\psi} \psi^*(l') dl dl' - \frac{\bar{J}_{\phi}}{B_{\phi}} \oint \frac{\psi^* u' + \psi u'^*}{2} dl, \quad \psi \equiv -\frac{B_p r}{B_{\phi}} u' - i n u$$

High plasma T_{edge} in LiWF is consistent with the high performance spot on stability diagram

Quiescent period in JET ITB experiments is consistent with this theory



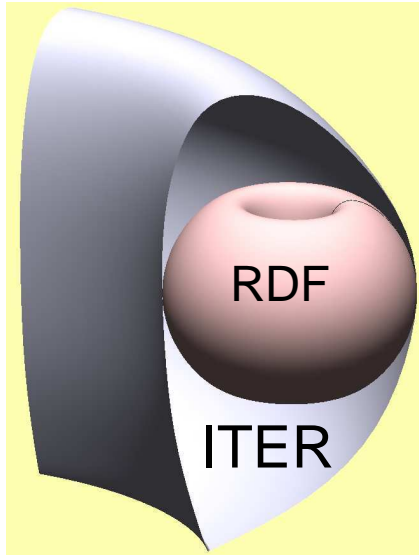
JET has a quiescent regime as transient phase from ELM-III to ELM-I

"Edge issues in ITB plasmas in JET"

Plasma Phys. Control. Fusion 44 (2002) 2445-2469 Y. Sarazin, M. Becoulet, P. Beyer, X. Garbet, Ph. Ghendrih, T. C. Hender, E. Joffrin, X. Litaudon, P. J. Lomas, G. F. Matthews, V. Parail, G. Saibene and R. Sartori.

The authors emphasized the crucial role of the edge current density

RDF is a powerful neutron source (0.2-0.5 GW) for reactor development

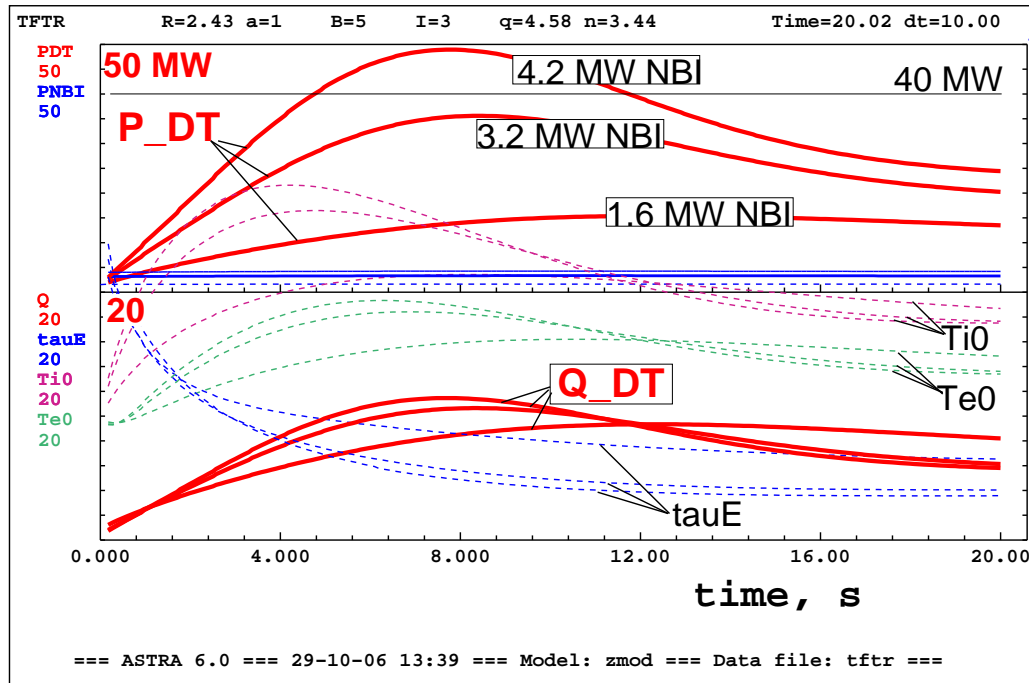


RDF should target three mutually linked objectives of magnetic fusion

1. *High power density plasma regime, $\simeq 10 \text{ MW/m}^3$*
2. *Fluence of neutrons 15 MWa/m^2 for designing the First Wall*
3. *Self-sufficient Tritium Cycle*

LiWF approach, together with existing technology, seems to be capable of accomplishing this mission

ASTRA-ESC simulations of TFTR, B=5 T, I=3 MA, 80 keV NBI



Even with no α -particle heating:

$$P_{NBI} < 5 \text{ [MW]},$$

$$\tau_E = 4.9 - 6.5 \text{ [sec]},$$

$$P_{DT} = 10 - 48 \text{ [MW]},$$

$$Q_{DT} = 9 - 12$$

within TFTR stability limits, and with small PFC load ($< 5 \text{ MW}$)

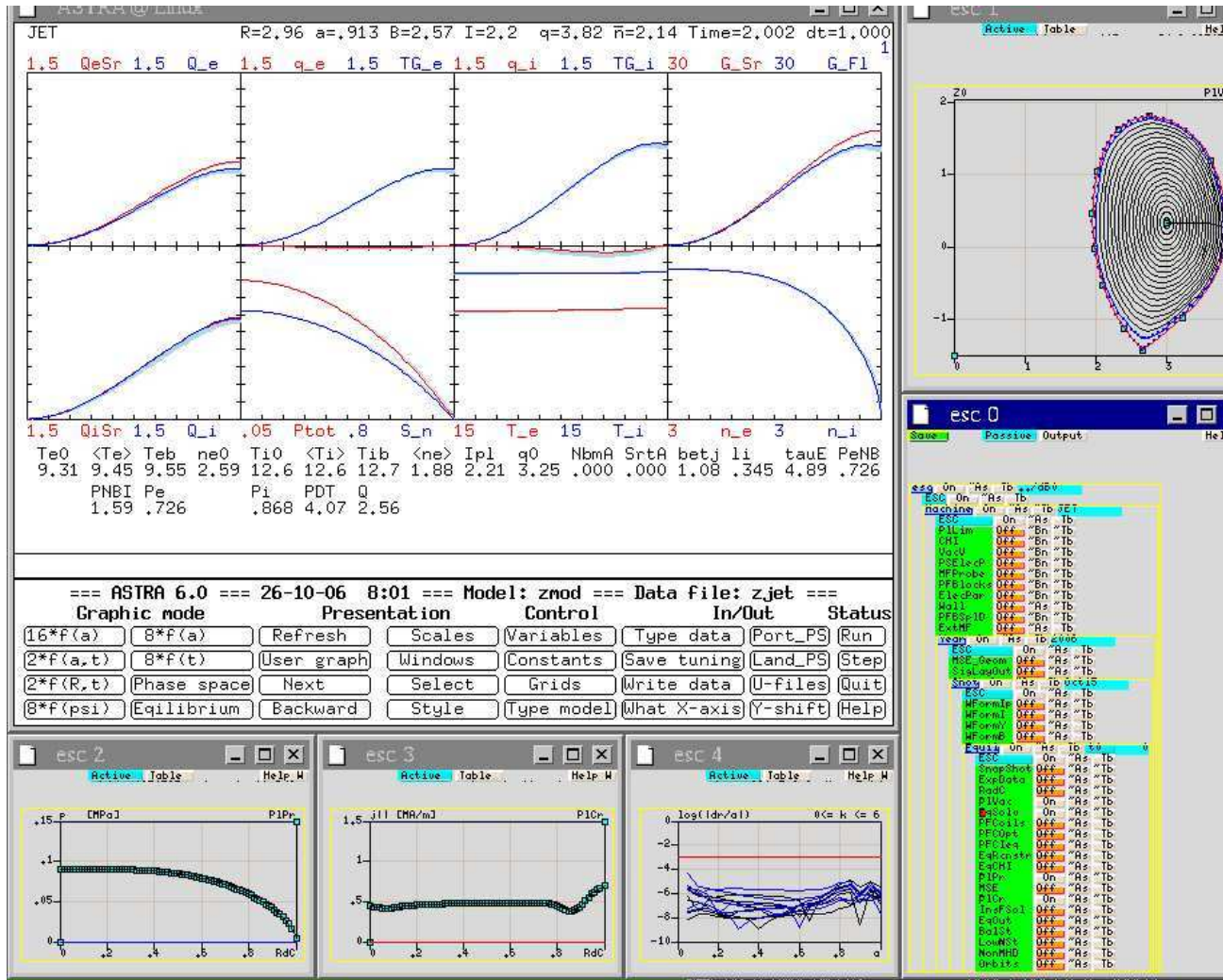
	PNBI	n	T	P DT	Q DT	tauE	nend	Ti0	Te0	gb %
(a)	1.65	0.3	10	15.4	9.34	6.54	0.42	18.7	14.8	1.64
(c)	3.30	0.3	10	35.5	10.6	4.04	0.55	17.6	13.6	1.96
(d)	4.16	0.3	10	48.9	11.6	3.58	0.59	17.5	13.4	1.96

The “brute force” approach ($P_{NBI} = 40 \text{ MW}$) did not work on TFTR for getting $Q_{DT} = 1$. With $P_{DT} = 10.5 \text{ MW}$ only $Q_{DT} = 0.25$ was achieved.

In the LiWall regime, using less power, TFTR could challenge even the $Q = 10$ goal of ITER

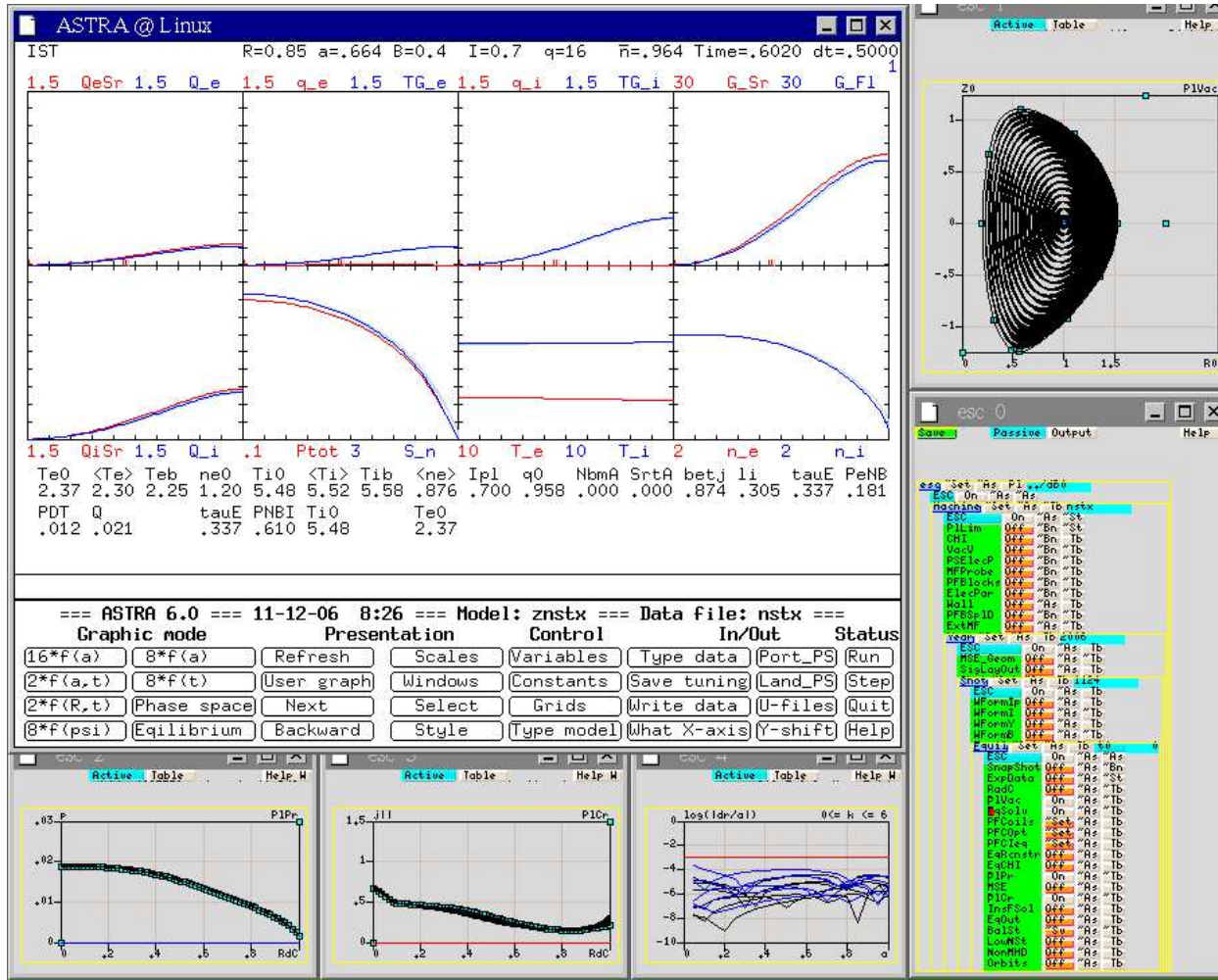
(Ignition criterion corresponds to $Q = 5$)

ASTRA-ESC simulations of JET, B=2.6 T, I=2.2 MA, 50 keV NBI



Can be experimentally tested on JET with intense Be conditioning

ASTRA-ESC simulations of ST-0, B=0.4 T, I=0.7 MA, 0.6 MW, 20 keV NBI



Hot-ion mode:

$$T_i = 5.5 \text{ [keV]},$$

$$T_e = 2.5 \text{ [keV]},$$

$$n_e(0) = 0.14 \cdot 10^{20},$$

$$\tau_E = 0.33 \text{ [sec]},$$

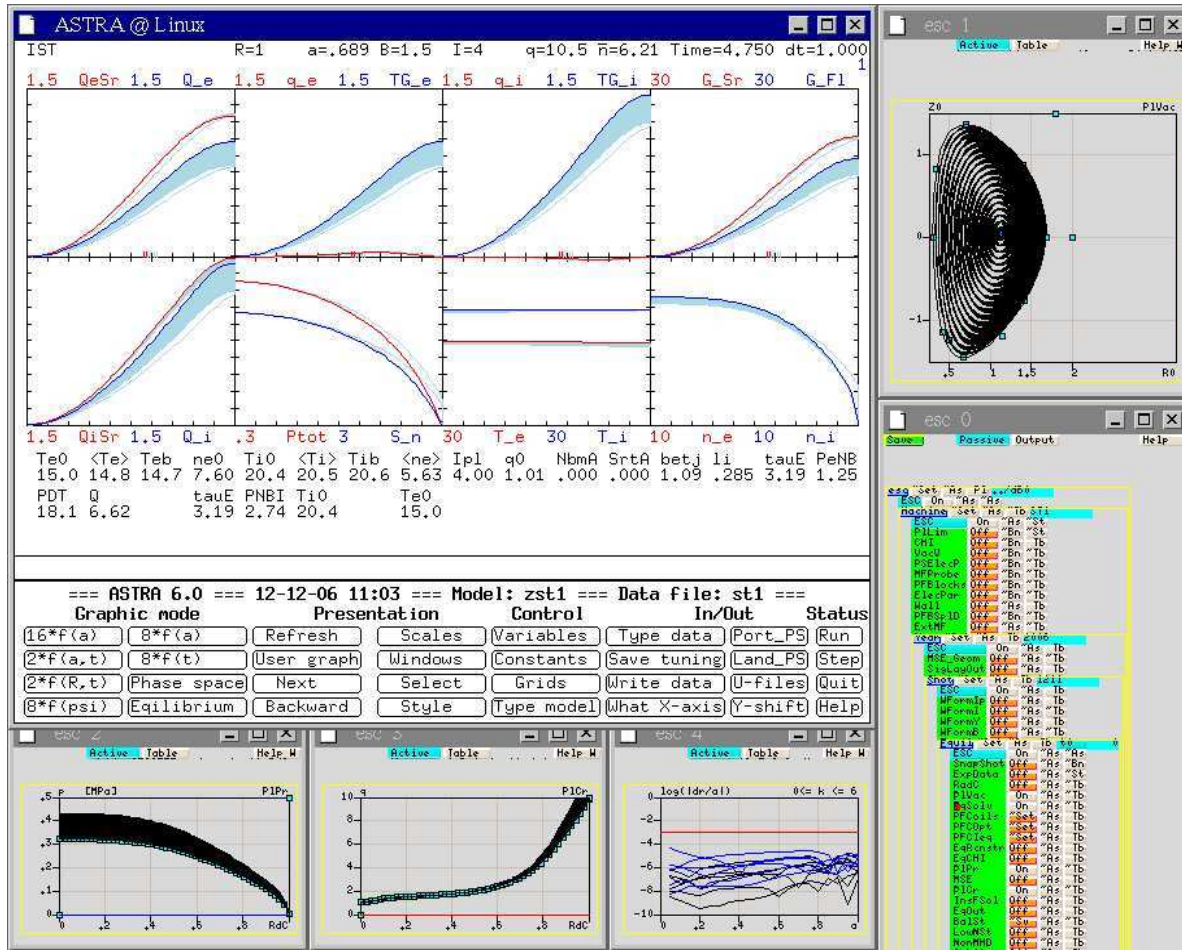
$$P_{NBI} = 0.61 \text{ [MW]}$$

NBI energy should be consistent with the plasma temperature:

$$E_{NBI} = 2.5(T_i + T_e)$$

ST0 should reach at least 1/3 of τ_E predicted by the Reference Model

ASTRA-ESC simulations of ST-1, B=1.5 T, I=4 MA, 2.7 MW, 80 keV NBI



Hot-ion mode:

$$\beta = 0.35,$$

$$T_i = 20 \text{ [keV]},$$

$$T_e = 15 \text{ [keV]},$$

$$n_e(0) = 0.75 \cdot 10^{20},$$

$$\tau_E = 3.19 \text{ [sec]},$$

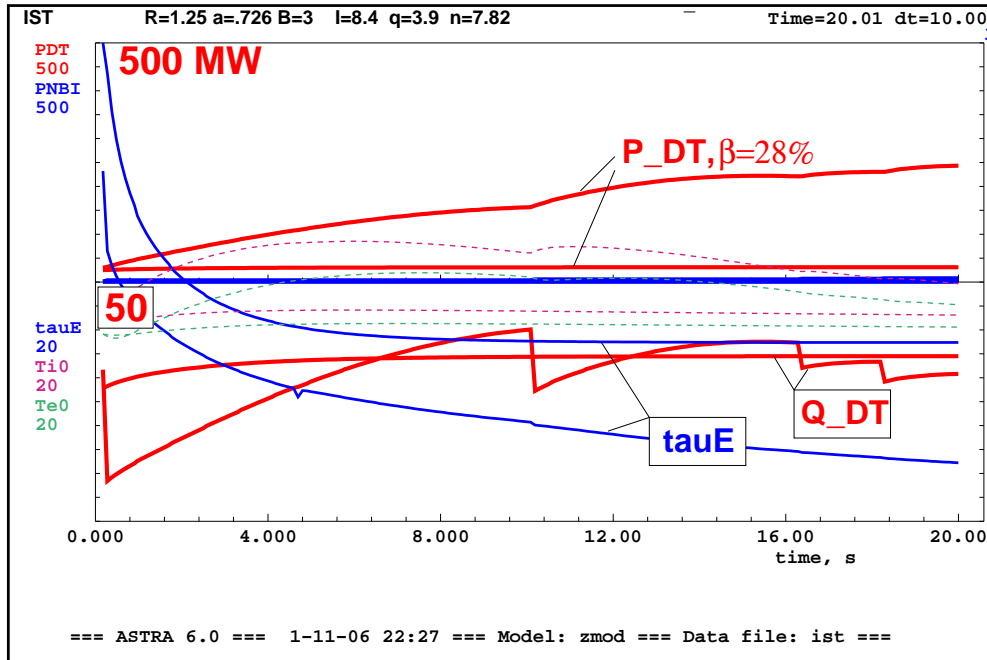
$$P_{\text{NBI}} = 2.7 \text{ [MW]},$$

$$P_{\text{DT}}^{\text{equiv}} = 18,$$

$$Q_{\text{DT}}^{\text{equiv}} = 6.6$$

ST-1 could be the first machine in super-critical regime, $Q_{\text{DT}}^{\text{equiv}} > 5$

ASTRA-ESC simulations of ST2, B=3 T, I=8.4 MA, 80 keV NBI



$$P_{DT}^{equivalent} \simeq 250 \text{ MW},$$

$$\beta = 28 \%,$$

$$Q_{DT}^{equivalent} \simeq 40,$$

$$P_{NBI} < 6 \text{ MW},$$

$$\tau_E = 5 - 16 \text{ sec}$$

The heat load of divertor plates is small

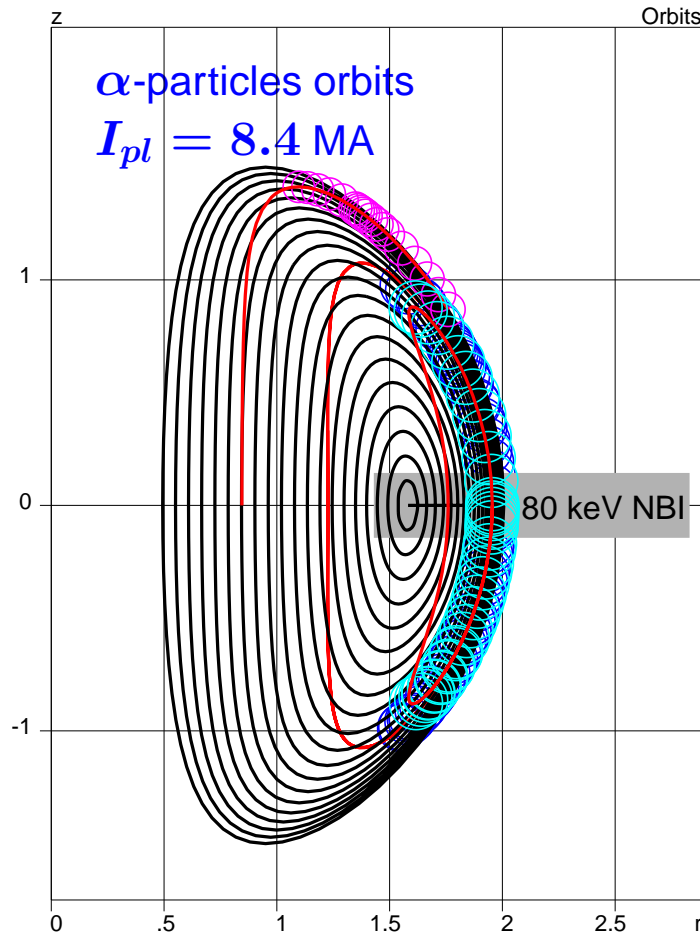
$$P_{NBI} \simeq 6 \text{ MW}$$

The regime of ST2 (with no fueling by tritium) is identical to RDF

The mission of ST2 is complete development of the stationary plasma regime for its DT-clone, RDF, (except extraction of α -particles).

Only LiWF approach allows the development of the full regime for RDF
even in Princeton area

Large Shafranov shift makes core fueling possible in RDF



The charge-exchange penetration length

$$\lambda_{cx} \simeq \frac{0.6}{n_{e,20}} \frac{V_b}{V_{b,80 \text{ keV}}} [m]$$

The distance between magnetic axis and the plasma surface in IST

$$R_e - R_0 = 0.3 - 0.5 [m]$$

**80 keV NBI can provide core fueling
and control of fusion power**

**Even at 8.4 MA 60 % of alphas intersect the plasma boundary
and can be intercepted at first orbits (e.g. by Li jets)**

Burn-up of tritium is proportional to the energy confinement time, and can be very efficient in LiWF

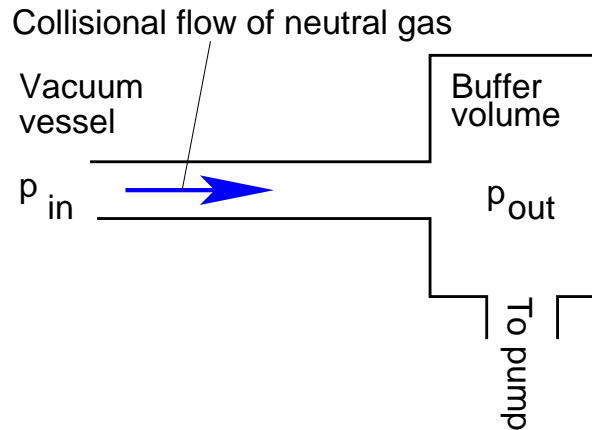
$$n \langle \sigma v \rangle_{DT,16keV} \bar{\tau}_E = 0.03 n_{20} \bar{\tau}_E$$

**In LiWF the burn-up of tritium could be a significant
fraction of unity**

On the other hand, due to reliance on ignition criterion $nT\tau_E^*$

BBBL70 is locked into very low, 2-3 %, rate of tritium burn-up

Conventional approach is based on gas-dynamic method

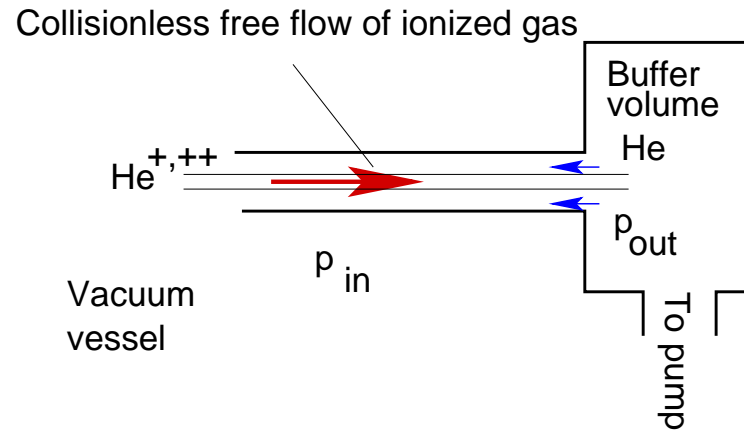


Dominant gas-dynamic scheme:

a) high pressure in the divertor

$$p_{in} > p_{out}$$

b) D, T, He are pumped out together



LiWall scheme:

a) Free stream of $He^{+,++}$ along B,

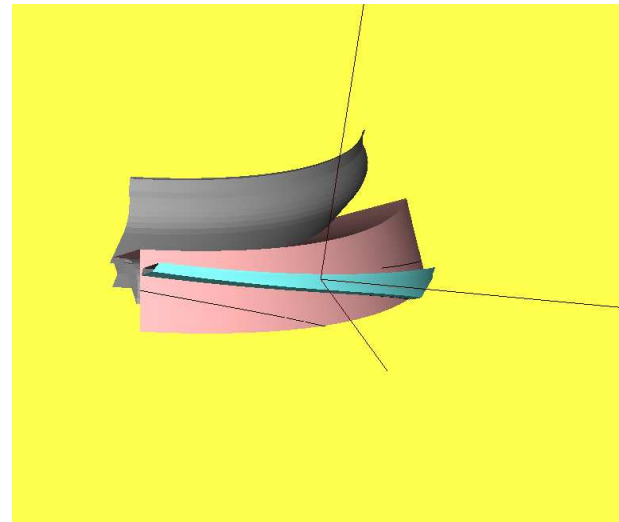
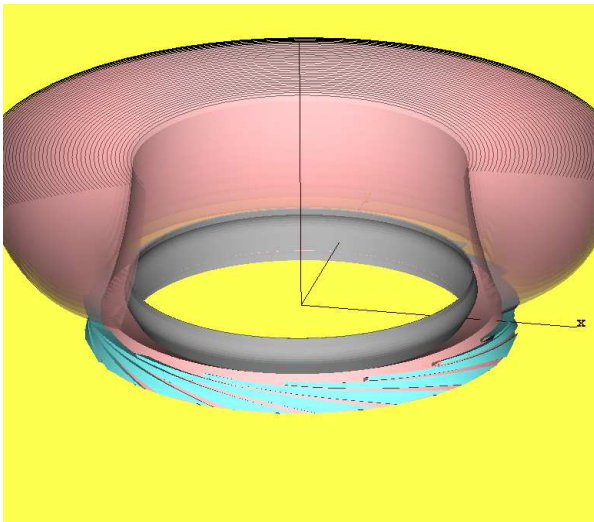
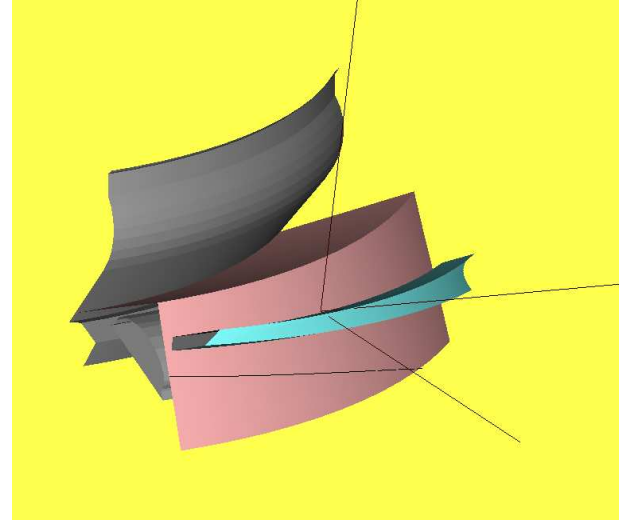
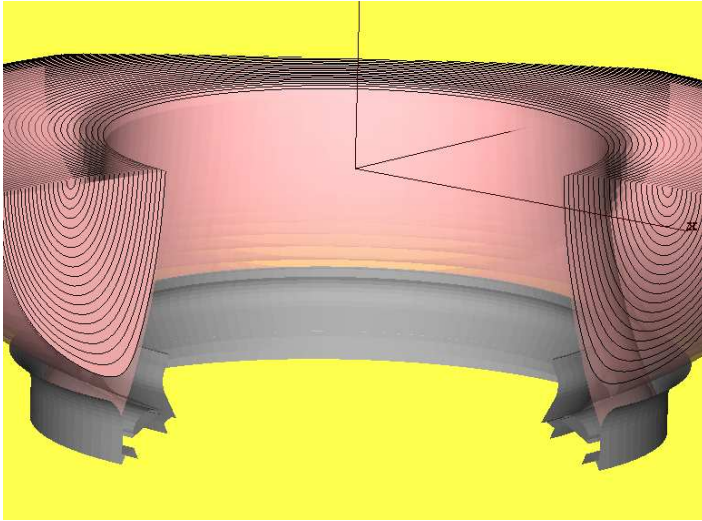
b) Back flow is limited by

$$\Gamma_{He} = Dn'_x, \quad D = hV_{thermal}$$

c) Helium density in the vessel plays no role, while D is in the hands of engineers.

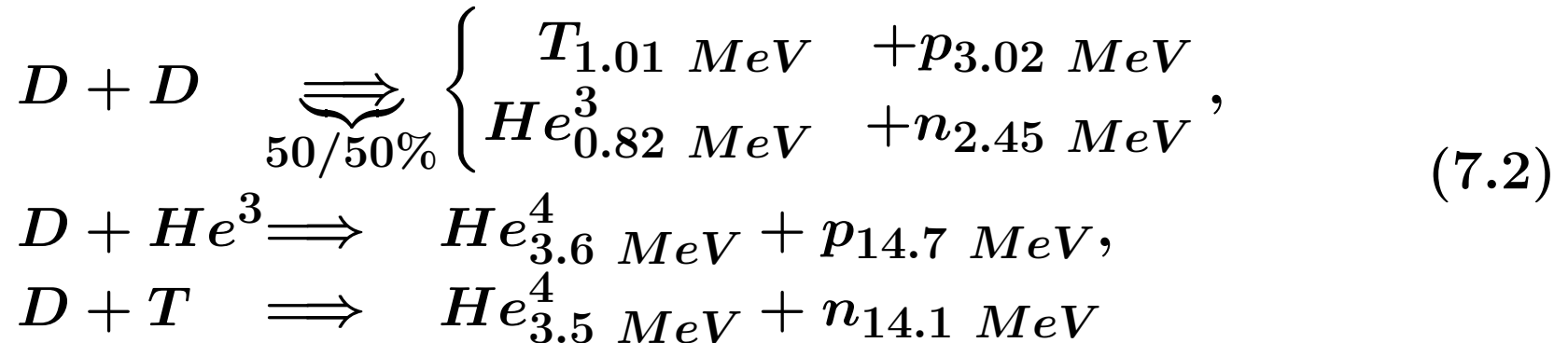
The second scheme is appropriate for the low recycling regime

Honeycomb channel duct utilizes condition $B_{pol} \ll B_{tor}$



Hot-ion regime and expulsion of the fusion products is suitable for DD fusion

Fusion reactions



Ion Larmor radii of charged products

$$\begin{aligned}
 \rho_{T,cm} &= \frac{10}{B_T} \sqrt{3}, & \rho_{p,cm} &= \frac{10}{B_T} \sqrt{\{3, 14.7\}}, & \rho_{\alpha,cm} &= \frac{10}{B_T} \sqrt{3.5}, \\
 \rho_{He^3,cm} &= \frac{10}{B_T} \sqrt{1.23} & & \text{– can be confined}
 \end{aligned} \tag{7.3}$$

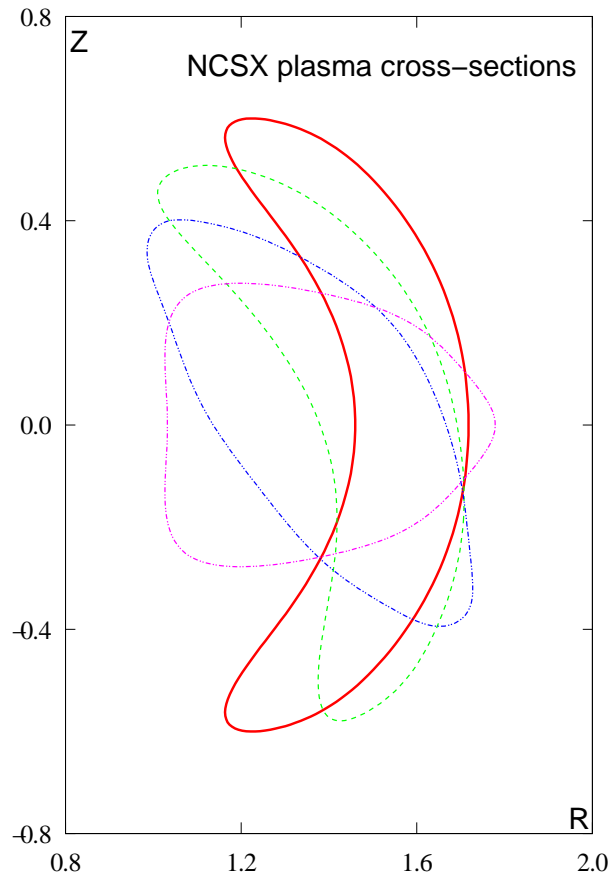
In $D + D, D + He^3$ fusion, the ash products have the same Larmor radii

$$\rho_{T,cm} \simeq \rho_{p,cm} \simeq \rho_{\alpha,cm} \tag{7.4}$$

and can be expelled on the first orbits.

LiWF is uniquely compatible with J.Sheffield's view on DD fusion

The 3 steps strategy has a vision beyond the RDF



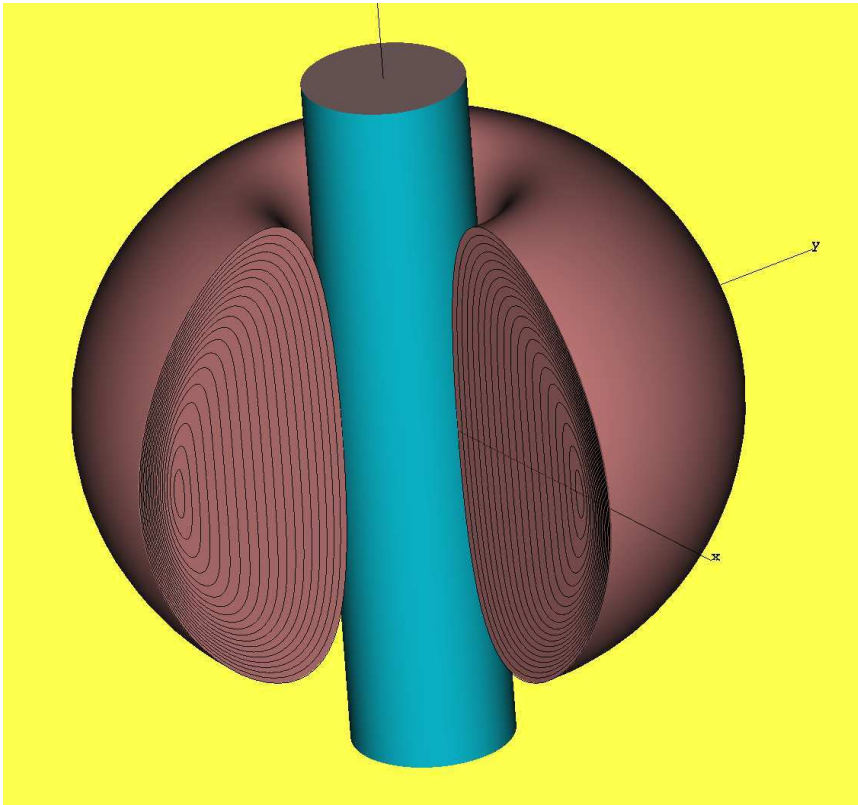
Regarding LiWall regime, Spherical Tokamaks are more similar to stellarators rather than to tokamaks:

- 1. Both are suitable for low energy NBI fueling*
- 2. Both are “bad” for α -particle confinement and good for SCD regime*

While STs cannot serve as a reasonable power reactor concept, the stellarators have no obvious obstacles to be a power reactor.

The LiWF strategy is consistent with both R&D and power production phases of fusion energetics

Spherical Tokamaks are the only candidate for RDF



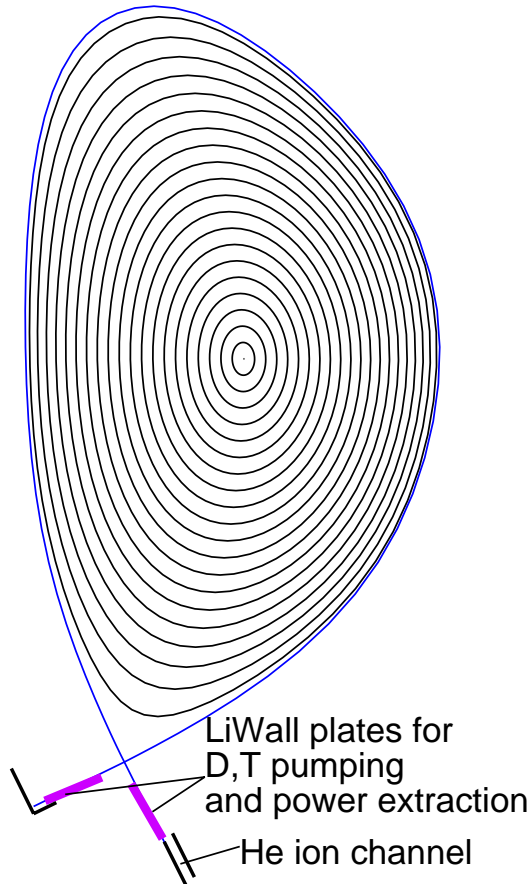
1. *Volume* $\simeq 30 \text{ m}^3$.
2. *DT power* $\simeq 0.2\text{-}0.5 \text{ GW}$.
3. *Neutron coverage fraction of the central pole is only 10 %*.
4. *FW surface area* $50\text{-}60 \text{ m}^2$

On properties of insulation, see [1] R.H. Goulding, S.J. Zinkle, D.A. Rasmussen, and R.E. Stoller, "Transient effects of ionizing and displacive radiation on the dielectric properties of ceramics," J. Appl. Phys. 79 (6), 2920 (1996).

**ITER-like device ($\simeq 700 \text{ m}^2$ surface)
would have to process
700 kg of tritium for developing
the First Wall.**

**The possibility of an unshielded copper central stack is
a decisive factor in favor of IST**

“Bleeding” (R. Goldston) Li target plate (belt limiter) with 0.1 mm thick Li is the concept of the pumping lithium divertor.



Replenishment of Li by gravity flow

$$\nu_{Pa \cdot sec} \simeq 5 \cdot 10^{-4}$$

$$V_g = \frac{\rho g h^2}{2\nu} \sin \theta \simeq 0.05 \frac{h^2}{0.01 \text{ mm}^2} \sin \theta,$$

Marangoni flow

$$\frac{d\sigma(T)}{dT} = -1.62 \cdot 10^{-4}$$

$$V_M = \frac{d\sigma(T)}{dT} \frac{h \nabla T}{\nu} \simeq 8 \cdot 10^{-5} \frac{h}{0.1 \text{ mm}} \nabla T$$

with Li supply controlled by capillary and wicking forces.

No rivers, water-falls of Li, evaporaton, dust, trays, or thick ($\simeq 1 \text{ mm}$) layers of Li on the target plates

Inventory of lithium for pumping purposes is not the issue

E.g., for the ITER size plasma 3-4 L of lithium ($0.1 \text{ mm} \times 30\text{-}40 \text{ m}^2$) with the rate of replenishment

$$10L/hour, \quad V_{Li} < 1 \text{ [cm/sec]}$$

is sufficient.

Existing technology of capillary systems (“Red Star”, T-11M, FTU, UCSD), gravity and Marangoni effect provide a solid design basis for pumping surfaces. Everybody has his own experience with solder and copper wire.

The issue is only in the oxidation (hydrolyzation) of the Li surface during the idle period of the machine.

**In LiWF molten lithium can be used to control the inventory
of unburned tritium**

There is very little in open literature on wetting/wicking by Li

The RDF program assumes conversion of NSTX in PPPL into ST0 with Li based PFC

- *The current NSTX program is essentially exhausted.*
- *It is focused mainly on self-improvements and is trailing the achievements of other teams, rather than advancing fusion energy.*
- *The program already has been twice explicitly warned about possible shutdown.*
- **On the other hand, the experience accumulated on NSTX, and the machine itself, are extremely valuable for developing the next steps in magnetic fusion.**

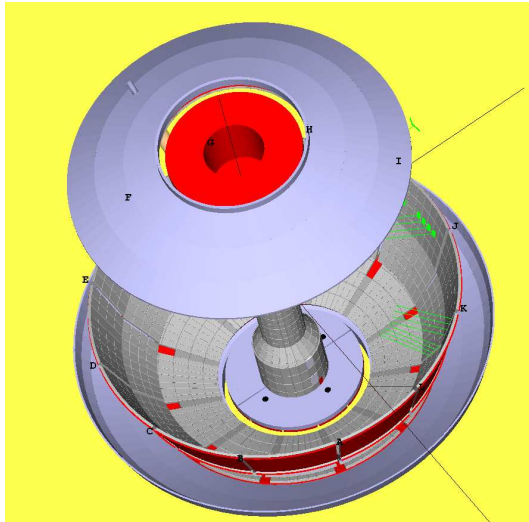
For ST0, the criterion for readiness of the machine to LiWall regime can be well-defined:

**Demonstration of complete depletion of the plasma discharge
by wall pumping, as on T-11M in 1998**

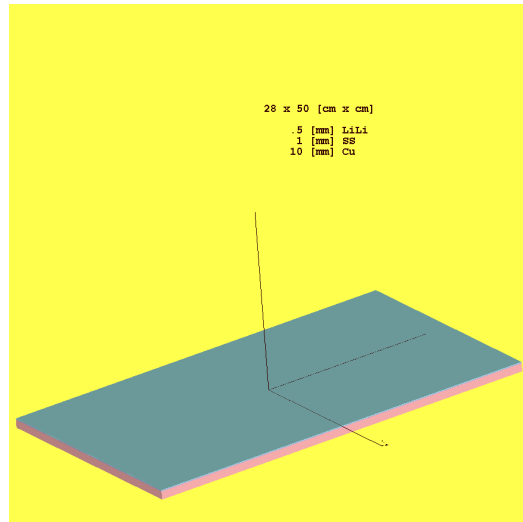
The mission of the ST0 is

**To demonstrate feasibility of the LiWall regime with
 $\tau_E \simeq 0.1 - 0.15 \text{ sec, } (\simeq 2 - 3\tau_{E,NSTX})$**

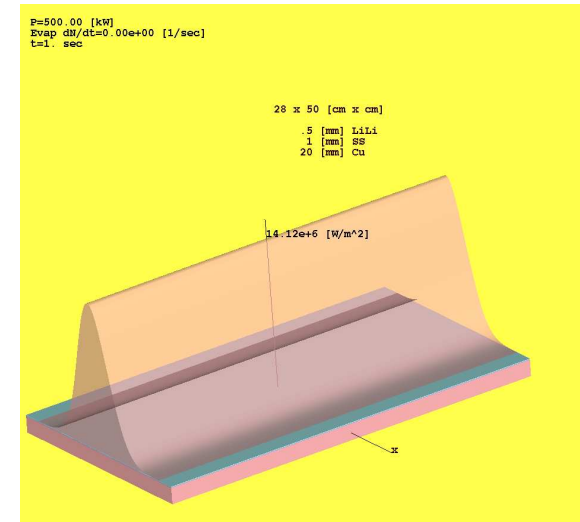
Molten Li is necessary to provide 10000 active monolayers or $\simeq 3\mu m$ of Li for pumping NSTX plasma



Li coated plate in low inner divertor



Li/SS/Cu (0.5mm/1mm/10mm) sandwich with a trenched surface

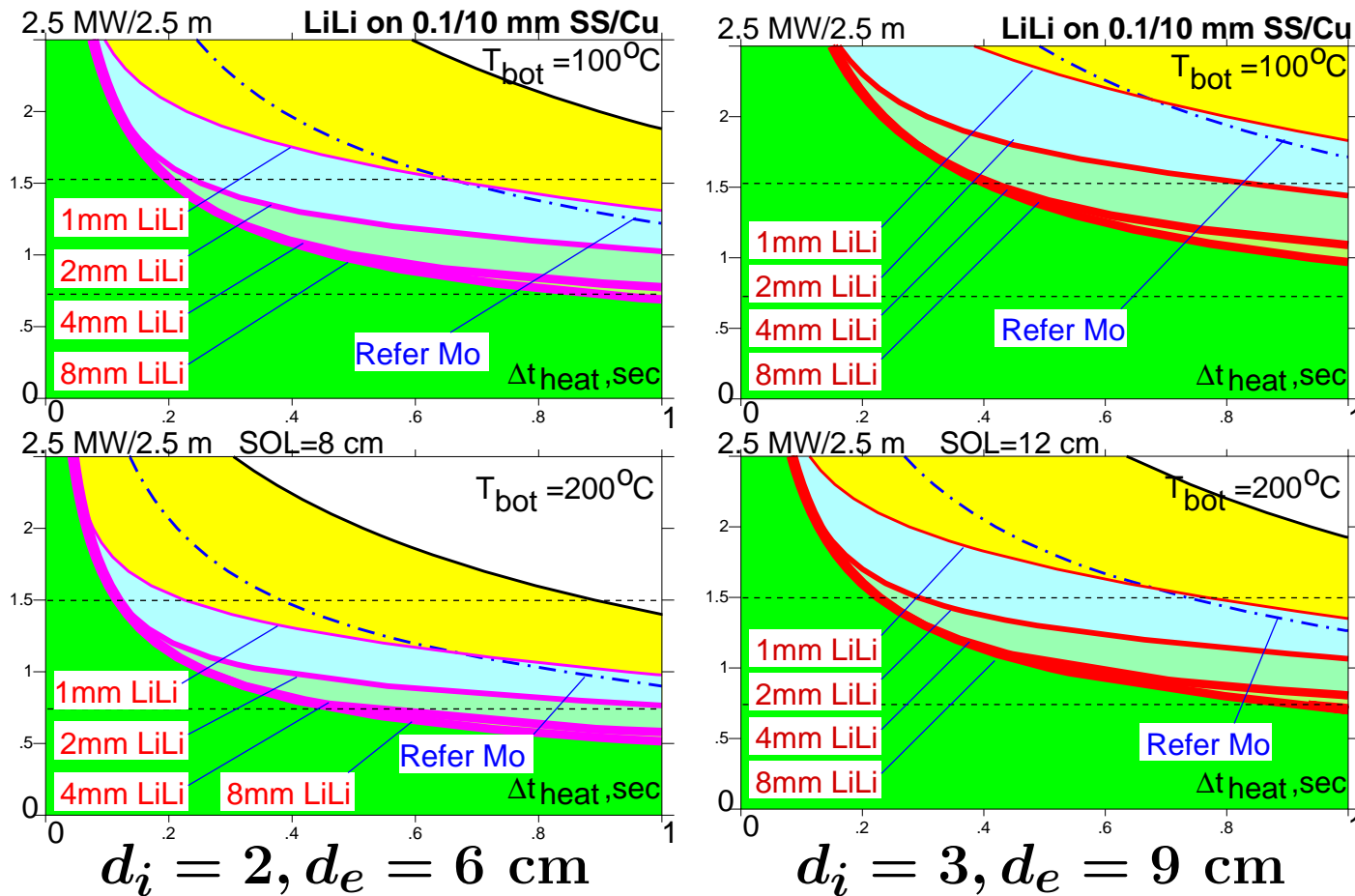


Gaussian (8 cm wide) heat deposition profile

$$\begin{aligned}
 S &\simeq 0.75 [m^2], \quad L_{SOL,m} = 2.5, \quad V_{Li} \simeq 0.35 [L], \quad M_{Li} \simeq 175 [g], \\
 \nu_{Pa \cdot sec} &\simeq 5 \cdot 10^{-4}, \quad I_{ion,MA} = \frac{(0.4 - 1) \cdot 10^{-3}}{1.6}, \\
 V_{Li,cm/sec} &= (2 - 5) \cdot B_{tor} \frac{h_{Li,mm}^2}{0.01} \frac{0.1}{w_{SOL}} \frac{I_{SoL,MA}}{I_{ion}}
 \end{aligned} \tag{7.5}$$

Li/SS/Cu plate could be the real first step toward Li PFC and LiW regime

The plate 0.1-1 mm of Li on 0.1/10 SS/Cu provides the operational space for the LiWall regime



Within 1-2 campaigns, experiments with plate could provide the data for ST0